



Application to the New
Hampshire Public Utilities
Commission

June 2013

TOWN OF PETERBOROUGH Photovoltaic Project Proposal



BORREGO SOLAR

6/7/2013



Letter of Transmittal

Borrego Solar, with its NH headquarters in Peterborough, NH, has teamed up with the Town of Peterborough to develop a 947kW ground mounted PV array to be located at the Peterborough Waste Water Treatment Facility (WWTF). The NH PUC has clearly stated that two of the most important selection criteria factors are the project's likelihood to expand the production capacity of renewable energy facilities in NH (including REC qualification) and the capacity of the team to successfully complete the initiative. After reading our proposal we hope you will share our belief that our team is extremely qualified and has the experience and expertise to complete this project.

This solar project will be a class I REC producing site, generating an estimated 1,150 REC's in the first year. Borrego Solar has provided a detailed production estimate using the industry standard PVSyst software. Borrego Solar has essentially written the book on production estimating – see SolarPro article – **Exhibit E**. Our fleet of systems has historically produced at 103% of estimated production, and we will have a production guarantee in our PPA with the Town of Peterborough. That guarantee includes damages should the system under-perform, which ensures our commitment to hitting the annual production estimates.

The Town of Peterborough has recently completed a state of the art WWTF at 58 Water Street. The new facility eliminates the need to have several acres of holding ponds. The waste from the ponds will be removed, and the ponds will be filled in. The solar project has been sited on top of one of the former ponds. The fill being brought in will ensure that the site is completely flat, making it an ideal site for a ground mount. The site is located directly adjacent to the WWTF. Half of the electricity will supply the WWTF and the other half will supply the Middle School across the street.

Borrego Solar is one of the largest solar developers in New England. We have constructed over 66MW's of projects financed under a Power Purchase Agreement structure. We have an impeccable track record of getting projects financed, and we have detailed our financing plan in section F. In our resume section you can see some of our recently completed PPA projects which include Easthampton, MA, Assumption College, Dartmouth, MA, Boston College High School and Mashpee High School.

Sincerely,

Joe Harrison – Senior Project Developer and Project Lead

Borrego Solar – jharrison@borregosolar.com (207) 432-1317

A. Summary of Proposal

Project Name:	Town of Peterborough – WWTF Solar Project	
Project Team (name, role):	<ol style="list-style-type: none"> 1. Joe Harrison – Senior Project Developer – Borrego Solar 2. Miles Hovis – Project Developer – Borrego Solar 3. Bryan Morrison – Engineering Lead – Borrego Solar 4. Joe Busch – Director of Operations – Borrego Solar 5. Rodney Bartlett – Town of Peterborough DPW Director 	
Project Location:	58 Water Street Peterborough, NH	
Technology Employed:	Photovoltaic System	
Brief Project Description: <i>(please include project life, in years)</i>	A 947kW (DC), 666kW (AC) ground mounted solar array to be installed at 58 Water Street in a former retention pond at the Town's Waste Water Treatment Facility. The project will be financed through a Power Purchase Agreement, the length of which will be 20 years with (2) 5 year extension options. The solar modules will be warrantied for 25 years, and this project should continue to produce for 30+ years.	
Capacity and Energy:	947 (kilowatts)	1,150,520 (kWh/year)
Total Project Cost:	\$2,626,495	
Total Funding Requested under this RFP:	\$1,340,000	
Economic Development Benefits:	Approximately 35 part-time jobs will be created and 50 full-time jobs will be supported by this project (including jobs created/retained)	
Environmental Benefits:	<p>2,289,515 Tons of CO₂e avoided/yr</p> <p>64,457 Gallons of fossil-fuel displaced/yr reduction, kW)</p>	
Anticipated Project Completion date:		

B. Technical Project Proposal

a. Overview of project

The project is sited directly adjacent to the brand new town owned waste water treatment facility. This new facility is state of the art and replaces acres of retention ponds. The first retention pond to be filled in is where the solar will be sited. Clean fill will be brought in to bring the site up to grade, creating a completely flat site, clear of trees or any other shade, perfect for a solar array. The proposed operation date for this project is August 22, 2013.

Please see our preliminary layout included as **Exhibit A**. This preliminary layout is a conceptual plan showing the location of the array and the individual panels. The equipment being deployed is listed below.

SYSTEM OVERVIEW

Total System Size:	947.1 kW DC 500 kW AC
Approx. Total System Square Footage:	94,710 SF
PV Panels:	(3157) Yingli Y300
Inverters:	(2) AE 333kW
Racking System:	GROUND MOUNT @ 20°
Estimated Annual Production:	1,150,520 kWh

Borrego Solar only chooses the best of the best, and the equipment which has been selected for this project has all been vetted by our Resources Group. Our Resources Group is headed by our Chief Technical Officer, NH native, Chris Anderson. Chris's group spends their time managing an active list of products that are considered financeable. They only choose solar panel manufacturers and inverter manufacturers with a track record of success. One of the most important things they look at is their warranty, and we only select companies which back up their warranties either with a publically traded parent company or an insurance policy. The Yingli solar panel, SMA inverter system is our most common system. We have several MW's in the ground of systems with Yingli modules and AE inverters.

This project will be fixed tilt which means there are not any moving parts. The project will need relatively limited maintenance. We will monitor the system at all times and will respond to any issues.

Aerial Photo of Solar Array Area



b. Project ownership structure, including names of all project owners and project location ownership and/or leasing structure.

This project will be owned by Green Lake Capital (“GLC”), our sister firm and primary financing partner, through a single-asset limited liability company. GLC is entirely owned by Borrego Solar’s parent company, Walsin Lihwa. GLC will provide sponsor equity for a portion of the cost to develop, install and commission the project. The balance of the project cost will be funded by a tax equity investor and a term loan. We anticipate the investment structure will take roughly this form:

- 20% Sponsor Equity
- 40% Tax Equity Investor
- 40% Term Loan



The project's primary source of revenue will be the sale of electricity produced by the project through a fixed-term power purchase agreement (PPA) with the Town of Peterborough. Peterborough also owns the land on which the project will be constructed, and the project LLC will enter into a property lease with Peterborough set to match the term of the PPA.

Borrego Solar and Green Lake Capital have financed and constructed 46 MW of solar capacity together, a portfolio of projects worth \$203 million. The strength and stability of this partnership is a key differentiator in the solar finance industry, where projects are often orphaned for as project parameters evolve, incentive environments fluctuate, and investors back out. We have carefully calculated the level of NH PUC grant support needed to provide adequate returns for our investors, and we are confident that if we are awarded funding in the amount requested in this proposal, we will be able to move forward with the close of project finance without delay. At no time will finance be a barrier to this project's execution.

Borrego Solar's 30-year track record of sustainable growth makes us an ideal partner for the federal government. Our history and financial strength provide our customers with a credit profile and balance sheet they can trust. Since the inception of the Borrego Solar integrated PPA financing solution in 2009, we have closed seven separate solar funds and built strong relationships with banking partners to broaden our access to capital markets and bring in construction debt and tax equity financing to complement sponsor equity contributed by our parent company Walsin Lihwa.

c. Description of the project site's resource availability (i.e. wind resource, insolation).

In estimating the production of this system we chose the Concord, NH municipal Airport which provides National Renewable Energy Laboratory (NREL) TMY3 data. Our standard is to select the closest weather station to a site that offers TMY3 data which is why the Concord Airport was selected. Solar insolation is a measure of solar radiation energy received on a given surface area in a given time. It is commonly expressed as average irradiance in watts per square meter (W/m^2) or kilowatt-hours per square meter per day ($kW \cdot h / (m^2 \cdot day)$). At this site the annual horizontal global irradiation is 1385 $kWh/m^2/year$. When you divide this by 365 days/year you get an average daily irradiation of 3.79 $kWh/m^2/day$.



d. **Project timeline**, including start date, key milestones in project progress (design, permitting, construction, start-up, commissioning), and expected completion (project is operational) date.

We anticipate this project will take approximately one calendar year to complete, from the receipt of grant funding to the commercial operation date. A full schedule of anticipated milestones for this project is included at the end of this proposal in **Exhibit B**. Major milestone dates are listed below:

Project Milestone	Date
Grant Award & Contract Execution	July 26, 2013
Environmental Reviews and Permitting Complete	October 24, 2013
Utility Interconnection Agreement Executed	October 24, 2013
Construction Design Set Complete	November 13, 2013
Building Permit Received/Notice to Proceed Granted	December 10, 2013
Major Equipment Arrives at Site	March 10, 2014
Racking and Mounts Installed	April 9, 2014
Modules Installed/Substantial Completion	June 9, 2014
System Commissioning/Permission to Operate Granted	August 19, 2014
Project Close-out	August 22, 2014

Please note that these dates are preliminary, and subject to change based on grant funding and contract negotiation timelines, utility interconnection schedules, prolonged inclement weather, unforeseen site conditions, grid interruption, and other factors outside the scope of Borrego Solar's control.

e. **Assignment and roles** of individual key project personnel.

Peterborough WWTF Solar PV Project – Key Personnel

Key Personnel	Title/Role	Responsibilities	Company
Joe Harrison	Project Developer	Price Estimation, Modeling, Contract Negotiation	Borrego Solar Systems, Inc.
Miles Hovis	Sales Associate	Grant Application/ Proposal Creation	Borrego Solar Systems, Inc.



TJ Murphy	Applications Engineer	Technical, Performance, & Price Optimization	Borrego Solar Systems, Inc.
Rodney Bartlett	DPW Director	Facilities Management & Town Liaison	Town of Peterborough
Charlie Fitzgerald	Financial Analyst	Financial Modeling	Borrego Solar Systems, Inc.
Jason Tai	Managing Partner	Project Finance & Structuring	Green Lake Capital
Bryan Morrison	Engineering Lead	System Design, Permit Preparation	Borrego Solar Systems, Inc.
David Albrecht, P.E.	Civil Engineer	Permit Application, Environmental & Regulatory Compliance	Borrego Solar Systems, Inc.
Anne Dunbar	Electrical Engineer	Wire Management, Electrical Code Compliance	Borrego Solar Systems, Inc.
Scott Sargent	Project Manager	Construction Oversight, Permitting, Budget Control	Borrego Solar Systems, Inc.
Dan Stafford	Site Superintendent	Construction Oversight, Subcontractor Management	Borrego Solar Systems, Inc.
Gary Buchanan	Director of Operations & Maintenance	Ongoing System Monitoring & Management	Borrego Solar Systems, Inc.

f. Estimate of work to be performed in house and by sub-contractors and identify potential sub-contractors.

We anticipated that roughly 50% of the work performed on this project will be completed by full-time Borrego Solar employees. This includes the total number of hours devoted to the project by development staff, engineers, construction managers, and legal, administrative, accounting and executive personnel time. The remaining 50% will be performed by local electrical and civil sub-contractors, engineers and providers of ancillary site services.

g. Description of operation and maintenance plan for after the system has become operational, including estimated project lifespan.

While the PV modules we plan to deploy in this project have a warrantied life of 25 years, we anticipate this project will remain commercially operational for 30 years or longer, based on longitudinal studies of the performance of solar electric systems. Borrego Solar will provide with a comprehensive maintenance and monitoring plan to ensure the system's continuous operation. This offering will include the following duties and will be overseen by the Director of



Operation & Maintenance for Borrego Solar. Details of the personnel involved with this offering can be found in Section D of this application.

Operations and Maintenance Offering	
Service (Frequency)	Description
System Monitoring (Daily)	<ul style="list-style-type: none"> Borrego will monitor the system's performance online to check for warnings signs that the system is not producing at the expected levels (it being understood that "expected levels" or "as intended" as used herein means the System operating at projected production levels provided in the O&M Agreement). Planned monitoring solution is through Deck Monitoring (see included Deck Monitoring Overview.) The Deck platform provides an extensive equivalencies calculator which can be used to interpret cost impacts of outages and performance deviations. Multiple PV systems can be monitored through a single dashboard, allowing quick identification of low performing systems.
Remote Alerts and Diagnostics (As Needed)	<ul style="list-style-type: none"> Alerts will be automatically e-mailed to Borrego Solar (and select Client representatives if desired) in response to a variety of system performance issues, including low production, inverter outages, grid disturbances, and sub-combiner imbalances. A full suite of diagnostic tools is available within the Deck solution, allowing Borrego's O&M Department to drill down into historical and real-time system activity in order to best determine appropriate corrective and preventative activities.
Unplanned Outage Response (As Needed)	<ul style="list-style-type: none"> In response to remote system monitoring, system-generated alerts, or inquiries from Client personnel, remote analysis of system begins immediately. If analysis determines on-site inspection or corrective activities are required, Client would be notified of the planned arrival of service technicians, and a technician would be scheduled for onsite activity within 72 hours, if not sooner. All service cases and service visits are tracked in Borrego's CRM application through completion.
Site Inspection and Preventative Maintenance (Annually)	<ul style="list-style-type: none"> One scheduled washing of modules (# of washings can be increased as environment dictates). Visually inspect system for loose wiring or any other safety or performance hazards including tree growth Take and log current readings of all strings, instantaneous kW output of inverters, operating voltage at inverters, and cumulative kWh readings of all inverters Check home run wires (from PV modules to combiner box) at DC string combiner box to ensure there is no loose or disconnected wiring). Tighten any loose connections. Check all combiner fuses. Replace any blown fuses. Check that array frames, racks, metal boxes, etc. are connected. Ensure that all labels and safety signs specified in the plans are in place. Check all disconnect switches (from the main AC disconnect all the way through to the combiner box). Record any switches that need replacement. Visually inspect the array for cracked modules. Record the location of any modules needing replacement. Inspect site for indications of tree growth shading arrays and notify owner if tree maintenance is required. Check and confirm proper torque settings of wire terminations. Check and log Voc and Imp of all strings. Visually inspect system for loose wiring or any other safety or performance hazards including tree growth. Check calibration on weather sensors per manufacturer recommended schedules. Check calibration on meters per manufacturer recommended schedules. Visually inspect any plug and receptacle connectors between the modules and panels to ensure they are fully engaged. Tighten any loose connectors. Check that strain reliefs/cable clamps are properly installed on all cables and cords by pulling on cables to verify. Tighten any loose connections Perform Preventive Maintenance on inverters per manufacturer's instructions, including cleaning inverter air filters, verifying up-to date software releases, and verifying system is operating as expected. Create and issue written inspection report.



C. Qualifications and Experience

- a. **Qualifications, experience, and roles** of the project team with resumes of key personnel, including sub-contractors, if applicable. Resumes can be included as an attachment and do not count toward the page limit.

Please see the listing of project team members included in Section C above. Compressed resumes for key personnel can be found at the end of this grant proposal in **Exhibit C**.

- b. **The name, and contact information** of the person who has the authority to enter into a binding agreement.

Joe Harrison will be the primary point of contact for contract negotiations for Borrego Solar:

Joe Harrison
Senior Project Developer
Borrego Solar Systems, Inc.
1115 Westford Street, 2nd floor
Lowell, MA 01851
Mobile - 207-432-1317
Fax - 888-843-6778
MA License # 97365
jharrison@borregosolar.com

- c. **Summaries of similar projects** undertaken by key personnel (date of project installation, summary of project, client name, name and phone number of contact for reference).

Established in 1980, Borrego Solar Systems, Inc. is one of the nation's leading financiers, designers and installers of commercial and government grid-connected solar electric power systems. Borrego Solar's photovoltaic systems are efficient, reliable and cost-effective. With more than three decades of experience and more than 1,050 installations completed and under construction —totaling more than 150 MW—Borrego Solar offers a complete line of design and installation services throughout New England and the nation.



A.D. Makepeace

Cranberry Grower and Landowner

27 Charlotte Furnace Road

Wareham, MA 02576

System Size: 4.73 MW

Completed: 4/13/2012

Jim Kane

(508) 728-0476

jkane@admakepeace.com

- Yingli 230 W modules
- SMA Central Inverters
- Schletter Ground- Mount Solution
- PowerDash Monitoring System

***Financed via Borrego Solar's In-House PPA**



Harvard University

Gordon Indoor Track

65 North Harvard Street

Boston, MA 02163

System Size: 592 kW

Completed: 06/22/2012

Jon Lister, Assistant Director of Athletics

(617) 384-8426

jlister@fas.harvard.edu

- Yingli 260 W modules
- Satcon Central Inverters
- Panel Claw Rooftop Mounting Solution
- DECK Monitoring Solution



Sierra Community College District

1.275 MW installation across 2 campuses

Completed: 10/7/2011

Laura Doty, Director, Facilities and Construction

(916) 660-7650

ldoty@sierracollege.edu

- Yingli 260 W modules
- Satcon Central Inverters
- Custom Support Structures
- DECK Monitoring Solution

***Financed via Borrego Solar's In-House PPA**





City of Easthampton Landfill

Ground-mounted installation on landfill

200 Oliver Street

Easthampton, MA 01027

System Size: 2.26 MW

Completed: 12/23/2011

Michael Tautznik, Mayor

(413) 529-1470

miket@easthampton.org

- Yingli 235 W modules
- SMA Central Inverters
- Solar FlexRack Ground- Mount Solution
- Power One Aurora Vision (DAS)

***Financed via Borrego Solar's In-House PPA**



TMLP – Padelford Street

Ground-mounted installation

32 Padelford Street

Berkley, MA 02779

System Size: 2.16 MW

Completed: 12/14/2012

Steve D'Angelo

(508) 942-3733

lynne.dangelo@yahoo.com

- Yingli 240 W – 265 W modules
- SMA Central Inverters
- Terra Farm Ground- Mount Solution
- Revenue Grade DAS



Reed Road Solar Farm

Independent Developer

968 Old Reed Road

Dartmouth, MA 02747

System Size: 1.30 MW

Completed: 5/25/2012

Peter Hawes

(508) 965-0253

peterland@comcast.net

- Yingli 235 W modules
- SMA Central Inverters
- Schletter Ground- Mount Solution
- PowerDash Monitoring System

***Financed via Borrego Solar's In-House PPA**





D. Renewable Energy Generation and Capacity *(1 page, not including model results and charts)*

a. Projected Kilowatt hours (or Btus where applicable) generated (annual and lifetime).

1,196,990 kWh in year 1 and 22,412,722 kWh over the initial 20 year life of the project.

b. Power capacity in kW (AC and DC) or kW equivalent (nameplate, gross and net capacities).

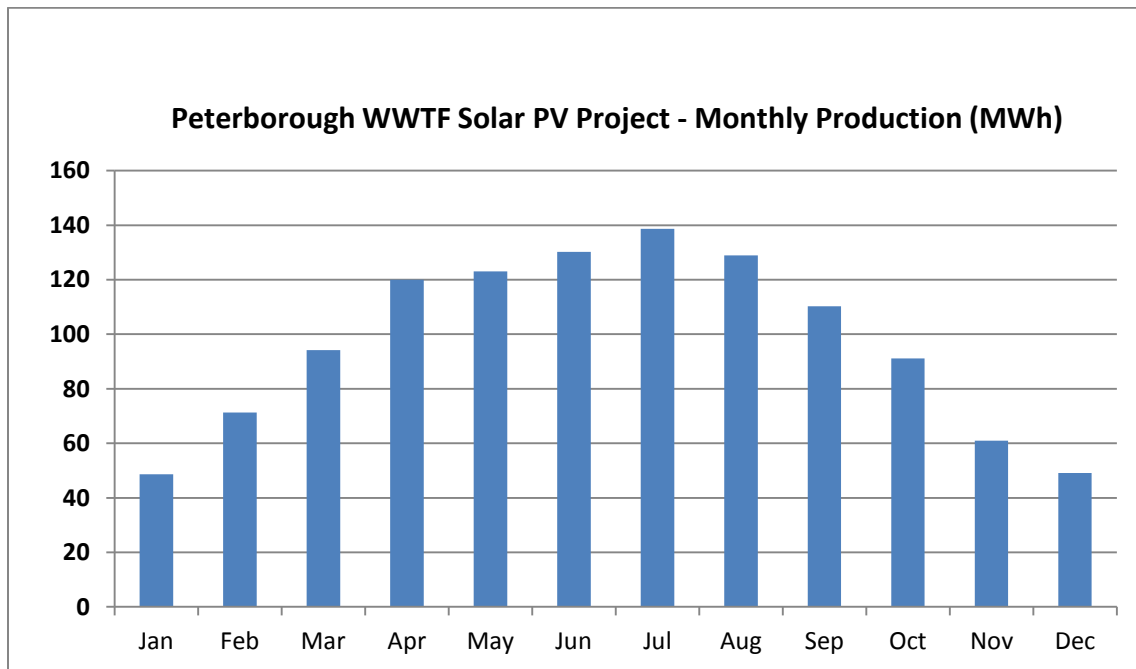
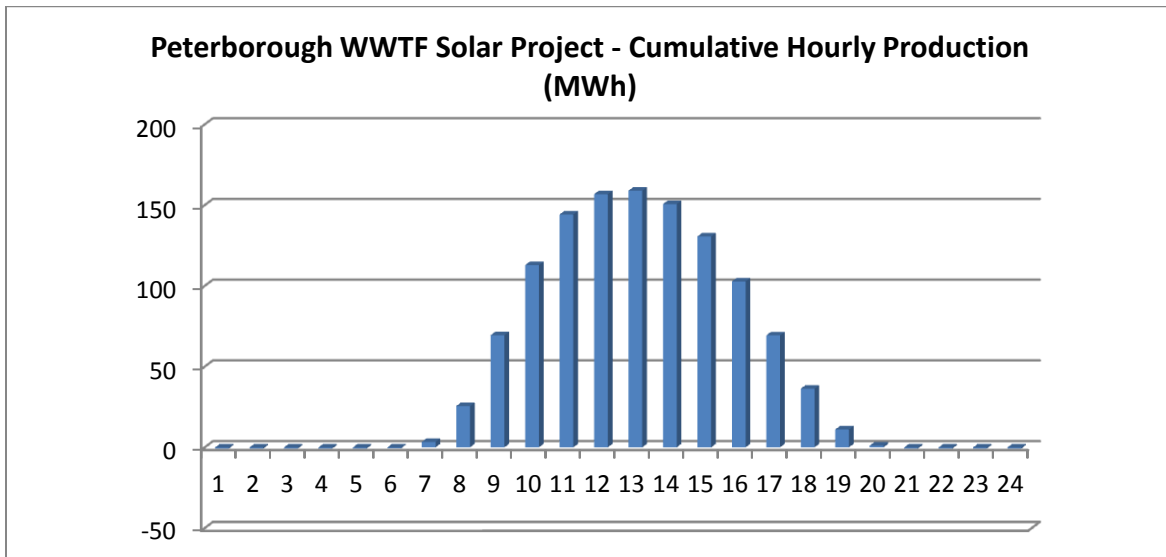
947kW (DC) and 666kW (AC)

c. Modeling results of expected gross and net capacities and estimated annual energy production.

Please see our PVSyst report attached as **Exhibit D**. The expected year 1 production is 1,150,520 kWh.

d. Daily, monthly, and annual load curves.

Daily and monthly load profiles for the Peterborough WWTF solar PV facility are summarized in the graphs below. More detailed load profile projections are included with the PVSyst report at the end of this proposal in **Exhibit D**.



e. Projected increase in annual supply of NH renewable energy credits (RECs), by class, resulting from project.

The project is projected to produce 1,150 class I REC's in year 1.

E. Cost & Financing (no more than 3 pages)

a. **Total project cost estimate**, itemized for equipment, labor, design, permitting, balance of system costs, etc.

BUDGET DATA			
Description	Category	Amount	\$/Watt
Modules	Materials	708,750	\$ 0.75
Inverter and Inv Warranty	Materials	202,950	\$ 0.21
Racking	Materials	280,000	\$ 0.30
Electrical Materials	Materials	17,394	\$ 0.02
DAS	Materials	22,092	\$ 0.02
Other Materials	Materials	0	\$ -
Carpot Materials	Materials	0	\$ -
Utility Materials	Materials	0	\$ -
Site Supervision & PM	Subcontractors	0	\$ -
Engineering	Subcontractors	20,427	\$ 0.02
Subcontractor Solar Install	Subcontractors	642,863	\$ 0.68
Roofing	Subcontractors	0	\$ -
Carpot Construction	Subcontractors	0	\$ -
Excavation/Grading/Trench	Subcontractors	140,000	\$ 0.15
Other Subcontractor	Subcontractors	37,620	\$ 0.04
Utility Labor	Subcontractors	10,000	\$ 0.01
Permits	Other	49,020	\$ 0.05
Bonds & Insurance	Other	0	\$ -
Other	Other	13,142	\$ 0.01
Contingency	Other	20,000	\$ 0.02
Referral Fees	SGA	0	\$ -
Financing	SGA	0	\$ -
Overhead	Overhead	150,662	\$ 0.16
		2,314,921	
Transaction Costs	SGA	135,600	\$ 0.14
Net Margin		\$175,974	\$ 0.19
		2,626,495	Final Price



b. The project's financing plan, description of financing status, and letters of intent/commitment from 3rd party financiers, if applicable.

Per the ownership structure described in Section C above, financing for this project is being secured by Borrego Solar's sister company, Green Lake Capital, which is wholly owned by Borrego's parent company, Walsin Lihwa. This in-house approach gives Borrego the ability to finance solar PV installations without bringing in a third-party to the negotiations, leaving it between Borrego (serving both the financier and design-build firm roles) and the Town of Peterborough. It also eliminates the risk of an otherwise viable project being orphaned when an energy provision contract is signed before committed investors are identified and funds allocated, which is the practice of many of our PV solar competitors.

The combination of sponsor equity commitment from our parent company along with our integrated EPC-PPA model will allow Borrego Solar to also reduce risk by eliminating the friction points that usually exist between the developer, EPC and investor. Our business model removes a costly duplication of efforts that typically exist in solar PPA financing. As a result we are able to offer our customers extremely competitive pricing and, just as importantly, high certainty of execution.

PPA Provider Capabilities	EPC Capabilities	Typical Areas of Overlap and Waste
Project finance & capital markets	Engineering	Sales and project development
PPA Contracts	Construction	Legal and contracts
Asset Management	Procurement	Project management

Established in 1966, Walsin Lihwa is a \$6 billion publicly traded Taiwanese conglomerate. In addition to providing corporate financial support, Walsin Lihwa has the option to invest directly into all of Borrego Solar's PPA projects, and has been a primary source of sponsor equity in our portfolio through their dedicated PPA investment vehicle Green Lake Capital (GLC). As a result of this relationship, we have successfully financed and interconnected over \$225 million of solar PPA projects. Walsin Lihwa has committed to investing another \$100M in US Solar PPA projects with Borrego. With our current capital commitments, we anticipate bringing financing for an additional \$500M to the US market in the next two to three years.



c. Description of all other financial resources, including grants, rebates, tax credits, etc.

In addition to the grant funding we seek from the New Hampshire PUC, we anticipate the following funding sources to support the development and construction of this project:

- The Federal Investment Tax Credit (ITC), accelerated depreciation, and other tax attributes of the investment, consumed by our tax equity investor
- Class I Renewable Energy Credits (RECs), which we value at \$0.04/kWh for a contractual term of 3 years
- The sale of solar energy to the Town of Peterborough on a \$/kWh basis over the term of a 20-year power purchase agreement (PPA)

d. Levelized cost of kWh, or thermal equivalent, produced (over lifetime of project).

The levelized cost of power (LCOE) over the life of this project, measured in \$/kWh over the course of the 20-year PPA and lease agreement with Dartmouth College, is as follows:

Funding Scenario	Levelized Cost of Energy (LCOE) (\$/kWh)		
	20 Years (PPA Term)	25 Years (Module Warranty)	30 Years (Anticipated Productive System Life)
NH PUC Grant Funding Awarded at Requested Level	\$0.0250	\$0.0203	\$0.0171
No NH PUC Grant Funding Awarded	\$0.0861	\$0.0697	\$0.0588



e. Projected Return on Investment (ROI) or Net Present Value (NPV) of project, with and without requested grant funding.

Funding Scenario	Net Present Value (NPV) at 5%
	20 Years (PPA Term)
NH PUC Grant Funding Awarded at Requested Level	\$2,846,065
No NH PUC Grant Funding Awarded	\$2,294,350

F. Potential Environmental, Economic Development and Societal Benefits (no more than 2 pages)

a. Environmental benefits

i. Fossil-fuel displaced (shown in gallons of oil, Tcf of natural gas, tons of coal, kWh)

It would require the burning of 67,850 barrels of oil to produce as much electricity as this solar system.

ii. Tons of CO₂e avoided and/or reduced

This solar system will reduce Carbon Dioxide emissions by 45,790,311 lbs.

iii. Emissions rates for thermal projects fueled by biomass

Not applicable.

b. Economic Development

i. Direct jobs created

There are about 35 part time jobs created.

Borrego directly employs

Project Developer: 1-2 people

Design Engineer: 1-2 people

Structural Engineer: 1 person

Electrical Engineer: 1 person

Project Manager: 1 person

Site Superintendent: 1 person

Project coordinator: 1 person

Rebate administrator: 1 person

Monitoring & Maintenance: 2 people

Total of around 11 people (not including the accounting, HR, marketing legal, insurance, banking, and other ancillary services associated with the operation of the company)

Borrego Sub Contracts with

General contractors: 8-10 people

PV Installers: 20-24 people

Electricians: 10-12 people

Because it's a ground mount

Lanscapers: 8-10 people (maybe a few more if we need to do some hill work like leveling)

Welders: 4-6 people

Total of around 66 people (not including the accounting, HR, marketing legal, insurance, banking, and other ancillary services associated with the operation of the companies represented here)

Then there are the employees who work for the module, inverter, and racking manufacturers. The teamsters who deliver products to site, the hardware like nuts, screws, bolts, conduit, electrical cabling, etc that we need to purchase from local vendors and distributors.

On projects of this size we're usually having to rent large equipment (IE: fork lift, man lift, crane, etc). We have to hire labor to operate this equipment and deliver it to/from the site.

All this considered there are approximately 50 people employed full time for a minimum of 3 months.



ii. Jobs retained (please show justification for estimate).

There are approximately 50 people employed full time for a minimum of 3 months.

Borrego directly employs

Project Developer: 1-2 people

Design Engineer: 1-2 people

Structural Engineer: 1 person

Electrical Engineer: 1 person

Project Manager: 1 person

Site Superintendent: 1 person

Project coordinator: 1 person

Rebate administrator: 1 person

Monitoring & Maintenance: 2 people

Total of around 11 people (not including the accounting, HR, marketing legal, insurance, banking, and other ancillary services associated with the operation of the company)

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c. Societal Benefits



i. Description of any benefits to public or non-profit entities, reduction in peak load in New Hampshire, and potential of project to defer or eliminate local utility distribution plant expenditures.

Distributed generation solar PV systems are ideal additions to electricity distribution systems from the perspective of peak load reduction, in that periods of peak solar electricity production – sunny afternoons – correspond with periods of peak summer demand of the utility grid. We have included an hourly production profile summary for our proposed system along with our PVSyst annual production report in **Exhibit D**. ISO-NE defines the summer peak demand periods as weekdays, 1:00 p.m. – 5:00 p.m., June through August for the purposes of forward capacity generation and demand response. We have highlighted these hours in our hourly production model. Our system is projected to reduce the Town of Peterborough’s demand during this peak period by 176,010 kWh in its first year of operation. The system will reduce the Town’s demand by approximately 1,150,520 kWh in total in its first year, and 32,126,156 kWh over the course of our 20-year PPA with the College.

ii. Description of high performance design and/or energy efficiency components to the project or project site, if applicable.

This project is a fixed tilt solar array. The beauty of the design is that it has no moving parts. All of the components have long-term warranties from the manufacturer. The panels have a 25 year warranty. The system will also have a production guarantee from Borrego Solar, so the production estimates are guaranteed. Borrego Solar has more experience installing large-scale ground mounted systems than most any solar integrator in New England.

Borrego Solar only chooses the best of the best, and the equipment which has been selected for this project has all been vetted by our Resources Group. Our Resources Group is headed by our Chief Technical Officer, NH native, Chris Anderson. Chris’s group spends their time managing an active list of products that are considered financeable. They only choose solar panel manufacturers and inverter manufacturers with a track record of success. One of the most important things they look at is their warranty, and we only select companies which back up their warranties either with a publically traded parent company or an insurance policy. The Yingli solar panel, SMA inverter system is our most common system. We have several MW’s in the ground of systems with Yingli modules and AE inverters.



iii. Description of an educational component to the project, if one will exist upon completion.

Our project team believes it is imperative to educate the next generation on energy sustainability so they can contribute to the solutions to our world's energy and environmental problems. To this end, Borrego Solar has partnered with Real Curriculum to develop a series of lesson plans to educate K-12 students about solar electricity. The Solar Curriculum is a targeted set of lesson plans for primary, intermediate, and secondary grade levels that teach students how solar power works. Samples lesson plans can be provided at the Commission's request. We have partnered with several schools to create an integrated learning program for their students, using their solar project as a working laboratory for the study of renewable energy through dynamic monitoring platforms. If we are awarded the grant funding necessary to construct this project, we will work with the Town of Peterborough to develop a renewable energy education component to this project and share these resources with area primary and secondary schools.

H. Conflicts of Interest

i. Describe any potential conflicts of interest on the part of the project team or its sub-contractors.

There are no conflicts of interest that we are aware of.

Exhibit B

Peterborough WWTP Solar PV Project - Milestone Schedule

Project Milestones	Duration (Calendar Days)	Start Date	End Date
NH PUC Grant Funding Timeline	49	Friday, June 07, 2013	Friday, July 26, 2013
Grant Application Deadline	0	Friday, June 07, 2013	Friday, June 07, 2013
Application Evaluation & Project Selection	35	Friday, June 07, 2013	Friday, July 12, 2013
Grant Award & Contract Administration	15	Friday, July 12, 2013	Friday, July 26, 2013
Design & Permitting	137	Friday, July 26, 2013	Tuesday, December 10, 2013
Field Measurements and Site Investigation	7	Friday, July 26, 2013	Friday, August 02, 2013
Environmental Reviews and Permitting	90	Friday, July 26, 2013	Thursday, October 24, 2013
Utility Interconnection Agreement	90	Friday, July 26, 2013	Thursday, October 24, 2013
Civil/Structural/Electrical Engineering Investigation	7	Friday, July 26, 2013	Friday, August 02, 2013
50% Plan Set	28	Friday, August 02, 2013	Friday, August 30, 2013
Client Review Period on 50%	4	Friday, August 30, 2013	Tuesday, September 03, 2013
90% Plan Set	42	Tuesday, September 03, 2013	Tuesday, October 15, 2013
Final Client Review Period	4	Tuesday, October 15, 2013	Monday, October 21, 2013
Construction Set	21	Monday, October 21, 2013	Wednesday, November 13, 2013
Building Permit Review	25	Wednesday, November 13, 2013	Monday, December 09, 2013
Plans Approved & Notice to Proceed (NTP) Granted	1	Monday, December 09, 2013	Tuesday, December 10, 2013
Procurement	112	Tuesday, December 10, 2013	Tuesday, April 01, 2014
Racking Materials Order & Delivery	90	Tuesday, December 10, 2013	Monday, March 10, 2014
Inverters Arrive Order & Delivery	90	Tuesday, December 10, 2013	Monday, March 10, 2014
PV Modules Order & Delivery	90	Tuesday, December 10, 2013	Monday, March 10, 2014
Transformer Order & Delivery	98	Tuesday, December 10, 2013	Tuesday, March 18, 2014
Switchgear Order & Delivery	112	Tuesday, December 10, 2013	Tuesday, April 01, 2014
Construction Period	186	Monday, February 10, 2014	Friday, August 15, 2014
Review Construction Schedule with Subcontractors	7	Monday, February 10, 2014	Monday, February 17, 2014
Site Mobilization	7	Monday, February 17, 2014	Monday, February 24, 2014
Site Preparation	14	Monday, February 24, 2014	Monday, March 10, 2014
Install Racking and Mounts	30	Monday, March 10, 2014	Wednesday, April 09, 2014
Install PV Modules	30	Wednesday, April 09, 2014	Friday, May 09, 2014
PV Modules Wiring	30	Friday, May 09, 2014	Monday, June 09, 2014
Trenching & Conduit	7	Tuesday, April 01, 2014	Tuesday, April 08, 2014
Install Inverters & AC Equipment	15	Tuesday, April 01, 2014	Wednesday, April 16, 2014
Weather Impact Days	7	Wednesday, April 16, 2014	Wednesday, April 23, 2014
System Commissioning	30	Monday, June 09, 2014	Wednesday, July 09, 2014
Building & Safety Inspection	7	Wednesday, July 09, 2014	Wednesday, July 16, 2014
Utility Company Signoff	30	Wednesday, July 16, 2014	Friday, August 15, 2014
System Online	1	Friday, August 15, 2014	Friday, August 15, 2014
Project Close-out	7	Friday, August 15, 2014	Friday, August 22, 2014
Entire Project (from Contract Signing)	392	Friday, July 26, 2013	Friday, August 22, 2014



Peterborough WWTP Solar PV Project - Milestone Schedule

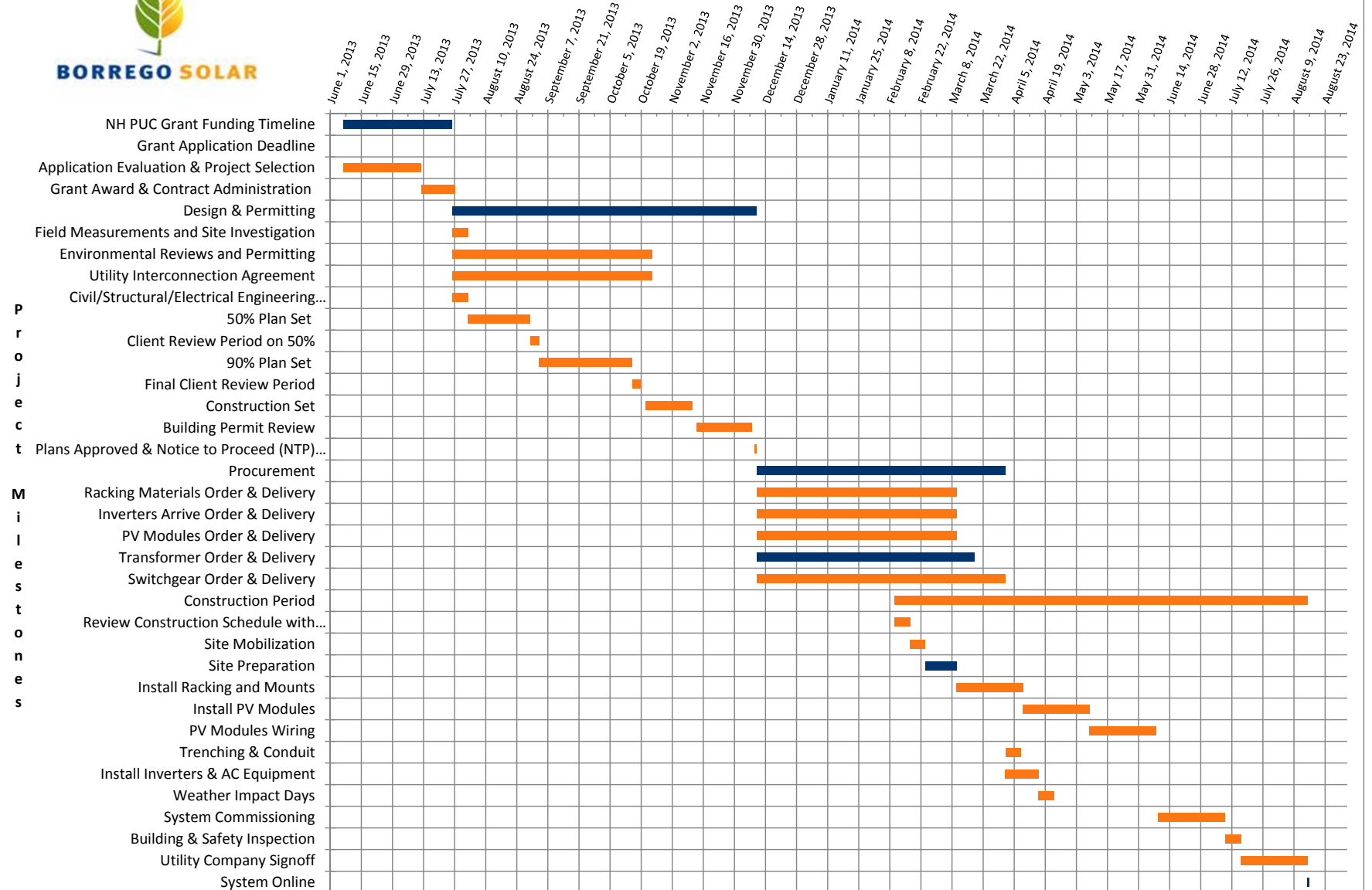


Exhibit C

Town of Peterborough, NH

NH PUC Grant Application

Key Personnel



Joseph Harrison

Senior Project Developer

Mr. Joe Harrison joined Borrego Solar in 2008 as a Project Developer. Joe's focus is on working with customers in the municipal and education sectors to implement comprehensive solar power solutions. Based out of Borrego Solar's regional headquarters in Lowell, MA, Joe has developed power purchase agreements (PPAs) for some of New England's most progressive municipalities, and largest K12 school districts, universities, community colleges, and private learning institutions. Joe's background in the fast-growing Massachusetts's solar market has made him the leader in solar for landfills, brownfields, and waste management centers. His experience has given him a greater understanding of the technical details associated with permitting for these sites, no-money-down solar financing mechanisms, solar renewable energy credits (SRECs), and the various incentives and subsidies available to schools and municipalities looking to go solar. Joe graduated from the University of Massachusetts with a Bachelor's degree in Business Management.

Thomas Murphy

Applications Engineer

Mr. Thomas Murphy serves as an applications engineer for Borrego Solar providing engineering and technical support, project assessment and cost estimation for Borrego's Eastern Project Development team. Thomas has worked in the solar industry since 2008 focusing on solar design, project management, site design and deployment of residential, commercial and large scale solar system. Prior to joining the solar industry, Thomas owned and operated a construction contracting business and held technical sales positions with software development firms in the Northeast. Thomas graduated from Fitchburg State University with a BS in Biology.

Miles Hovis

Sales Associate

Mr. Miles Hovis is a Sales Associate with Borrego Solar based out of the New England regional headquarters in Lowell, MA. Since joining Borrego Solar in 2010, Miles has worked to refine the company's competitive procurement response process. He is primarily responsible for proposal writing for projects in the Eastern United States, and manages inside sales company-wide. Additionally, Miles contributes to marketing, market research, and business strategy efforts for the East Coast project development team. Miles holds a Bachelor of Arts in anthropology from Brown University, where he also worked as an academic administrator before joining Borrego Solar.

Town of Peterborough, NH

NH PUC Grant Application

Key Personnel



Sam Chatterjee

Director of Project Finance

Mr. Sam Chatterjee is Director of Project Finance for Borrego Solar, working out of the regional headquarters in Oakland, CA. In addition to helping arrange conventional project financing for some of Borrego Solar's projects, Sam leads Borrego Solar's asset sales effort, focusing on finding buyers for projects in the company's development pipeline. His responsibilities in this role include identifying and building relationships with key buyers (both strategic players such as IPPs and financial partners such as private equity funds), running the process to market, identifying and selecting a buyer for particular projects and then negotiating key terms and conditions from a term sheet stage to contract signing and financial close. Previously, Sam led the monetization and risk management efforts on Borrego Solar's portfolio of solar renewable energy credits (SRECS). Prior to joining the Borrego Solar team, he worked in a Project Finance role at Solyndra where he was responsible for arranging lease and PPA financing deals originated by Solyndra's channel partners and direct end-users. Sam holds a Bachelor's of Engineering from the Birla Institute of Technology and Science, an MS in Computer Engineering from the University of Michigan, and an MBA from UC Berkeley's Haas School of Business.

Bryan Morrison

Lead Design Engineer

Mr. Bryan Morrison is the Lead Design Engineer for Borrego Solar's East Coast Operations. As a member of the engineering team, Bryan designs solar power installations that maximize production, efficiency and longevity for customers. As the East Coast Lead Design Engineer, Bryan produces detailed plan sets for commercial and public agency solar PV projects through the New England and Mid-Atlantic regions. Some of the most notable designs that Bryan has worked on to date include:

- City of Easthampton Landfill: 2.2 MW ground mount installation
- Roman Catholic Archdiocese of Newark, NJ: 1.662 MW across 11 sites
- Herring Properties: 1.24 MW ground mount installation

Scott Sargent

Project Manager

Mr. Scott Sargent is a Project Manager for Borrego Solar. Scott works with large-scale commercial and public-sector customers, overseeing and directing all activities related to a project's life cycle. This primarily includes the scope, schedule, and project-budget during engineering, procurement, construction, commissioning, testing, and project close-out. He manages the installation crews, project costs, and maintains quality control on site, liaising with the host customer along the way. He has managed the installation of multiple megawatts of solar PV throughout the Commonwealth of Massachusetts, and in 2011 he completed one of the largest solar landfill installations in the state.. Prior to joining Borrego Solar in 2008, Scott was an Iron Worker, Foreman, and Site Superintendent for a manufacturer of pre-engineered buildings.

Town of Peterborough, NH

NH PUC Grant Application

Key Personnel



Dan Stafford

Site Superintendent

Mr. Dan Stafford is a Site Superintendent based out of Borrego Solar's regional headquarters in Lowell, Massachusetts. As a Site Superintendent, Dan manages the construction of large-scale ground-mounted solar energy system by coordinating the joint efforts and needs of his customers, designers, project managers, and subcontractors. Dan has been working in solar since 2007 where he first worked in the residential solar power installations for Borrego Solar. Since then, he has installed more than 6 megawatts of PV in New England. He is a licensed Journeyman Electrician in Massachusetts, and waiting to sit for his Master Electrician License exam.

David Albrecht

Civil Engineer - P.E., C.E.

Mr. David Albrecht is a Civil Engineer for Borrego Solar. He is chiefly responsible for working with Project Developers and Project Managers on the civil engineering aspects of solar projects. David works to oversee civil engineering consulting contracts and also works with the Director of Engineering to further develop civil engineering design standards, site evaluation protocol and construction means and methods for Borrego Solar's Operations Team. David joined the company in 2012, having formerly worked as the Director of the Land Development Group at Tetra Tech, Inc. He holds Professional Engineers Licenses in four states and has completed several Project Management Training Programs. He had also completed the Franklin Covey and Dale Carnegie Leadership Trainings as well as the ACEC Leadership Course: Program for Emerging Leaders. David studied Civil Engineering Curriculum at San Jose State University, was an Engineer-Mentor for the Wilson Middle School Future City National Competition and is a Member of the Natick High School Building Committee.

David A. Dutil

Structural Engineer – P.E., S.E.

Mr. David Dutil is a Professional Structural Engineer for Borrego Solar. David is responsible for evaluating existing building structures as well as foundation systems and soil conditions for their ability to support a proposed roof or ground mounted solar array. He provides engineering feedback on racking designs and various installation components to make sure proposed systems are compliant with any load limitations and codes. Before joining Borrego Solar, David was a consulting structural engineer with Daigle Engineers, Inc. for seven years where he worked on a broad range of building-related design projects. David is currently licensed as a Professional Structural Engineer in Massachusetts and is a LEED® Accredited Professional. He earned his Bachelor of Science in Civil Engineering and Master of Science in Civil Engineering (Structural) from Rensselaer Polytechnic Institute.

Town of Peterborough, NH

NH PUC Grant Application

Key Personnel



Benjamin Walter

Lead Design Engineer – P.E., E.E.

Mr. Benjamin Walter is the Lead Design Engineer for Borrego Solar's West Coast Operations. Ben joined Borrego Solar in 2010 with a tremendous depth of solar PV design and engineering experience including the design of high-end building integrated (BIPV) systems, such as PV glass facades for skyscrapers and PV skylights. Ben leads the engineering effort on commercial and government projects nationwide, specializing in single-axis tracking designs. Ben is a certified Electrical Engineer and holds a Bachelors of Science in Electrical Engineering from the University of Akron, Ohio.

Gary Buchanan

Director, Operations & Maintenance

Mr. Gary Buchanan is the Director of Operations and Maintenance. As O&M Director, Gary oversees the daily monitoring and maintenance of all Borrego Solar's commercial and public sector installations using various data acquisition systems (DAS) and production forecasts. Gary has experience in all aspects of solar installation, service, and management, and is responsible for assuring Borrego's installed base of systems produce at or above the predicted levels of generation. His past experience in Telecommunications and IT Project Management made for a successful transition to solar in 2007. Since then, Gary has overseen the installation of over 3 megawatts of solar photovoltaic projects with a concentration on multi-family housing and educational markets. Gary has an Entry-level NABCEP certification and earned his Bachelor of Arts degree in Business and Computer Science from Rutgers University, New Jersey. He has also completed both basic and advanced solar PV design classes at Diablo Valley College in Northern California.

PVSYST V5.67		Duran Xiao, Walsin-IEI				05/06/13		Page 1/4																											
Grid-Connected System: Simulation parameters																																			
Project :		Peterborough DPW																																	
Geographical Site		Peterborough DPW				Country		USA																											
Situation		Latitude		42.9oN		Longitude		71.9oW																											
Time defined as		Legal Time		Time zone UT-5		Altitude		216 m																											
		Albedo		0.20																															
Meteo data :		Concord Municipal Arpt, NREL TMY3																																	
Simulation variant :		TERRASMART T25 A0 YL300 AE 333_060513																																	
		Simulation date		05/06/13 17h00																															
Simulation parameters																																			
Collector Plane Orientation				Tilt		25 deg		Azimuth		0 deg																									
5Sheds				Pitch		7.80 m		Collector width		4.04 m																									
Inactive band				Top		0.00 m		Bottom		0.00 m																									
Shading limit angle				Gamma		22.42 deg		Occupation Ratio		51.8 %																									
Shadings electrical effect				Cell size		15.6cm		Strings in width		12																									
Models used				Transposition		Perez		Diffuse		Measured																									
Horizon				Free Horizon																															
Near Shadings				Mutual shadings of sheds		Electrical effect																													
PV Array Characteristics																																			
PV module		Si-poly		Model		YL300P-35b BSS01																													
				Manufacturer		Yingli Solar																													
Number of PV modules				In series		22 modules		In parallel		143 strings																									
Total number of PV modules				Nb. modules		3146		Unit Nom. Power		300 Wp																									
Array global power				Nominal (STC)		944 kWp		At operating cond.		835 kWp (50oC)																									
Array operating characteristics (50oC)				U mpp		+/-358 V		I mpp		1164 A																									
Total area				Module area		6136 m2		Cell area		5511 m2																									
Inverter				Model		Solaron 333 BSS01																													
				Manufacturer		Advanced Energy Industries, Inc.																													
Characteristics				Operating Voltage		+/-330-550 V		Unit Nom. Power		333 kW AC																									
Inverter pack				Number of Inverter		2 units		Total Power		666 kW AC																									
PV Array loss factors																																			
Thermal Loss factor				Uc (const)		25.0 W/m2K		Uv (wind)		1.2 W/m2K / m/s																									
=> Nominal Oper. Coll. Temp. (G=800 W/m2, Tamb=20oC, Wind=1 m/s.)								NOCT		47 oC																									
Wiring Ohmic Loss				Global array res.		14 mOhm		Loss Fraction		2.0 % at STC																									
Array Soiling Losses				<table><tr><td>Jan.</td><td>Feb.</td><td>Mar.</td><td>Apr.</td><td>May</td><td>June</td><td>July</td><td>Aug.</td><td>Sep.</td><td>Oct.</td><td>Nov.</td><td>Dec.</td></tr><tr><td>24.3%</td><td>19.2%</td><td>15.8%</td><td>3.4%</td><td>0.9%</td><td>0.9%</td><td>0.9%</td><td>0.9%</td><td>0.9%</td><td>0.9%</td><td>5.3%</td><td>18.7%</td></tr></table>								Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sep.	Oct.	Nov.	Dec.	24.3%	19.2%	15.8%	3.4%	0.9%	0.9%	0.9%	0.9%	0.9%	0.9%	5.3%	18.7%
Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sep.	Oct.	Nov.	Dec.																								
24.3%	19.2%	15.8%	3.4%	0.9%	0.9%	0.9%	0.9%	0.9%	0.9%	5.3%	18.7%																								
Module Quality Loss								Loss Fraction		1.5 %																									
Module Mismatch Losses								Loss Fraction		0.5 % at MPP																									
Incidence effect, ASHRAE parametrization				IAM =		1 - bo (1/cos i - 1)		bo Parameter		0.05																									
System loss factors																																			
AC wire loss inverter to transfo				Inverter voltage		480 Vac tri																													
				Wires		29 m 3x500 mm2		Loss Fraction		0.5 % at STC																									
External transformer				Iron loss (24H connection)		1834 W		Loss Fraction		0.2 % at STC																									
				Resistive/Inductive losses		3.8 mOhm		Loss Fraction		1.5 % at STC																									

Grid-Connected System: Simulation parameters (continued)

User's needs :

Unlimited load (grid)

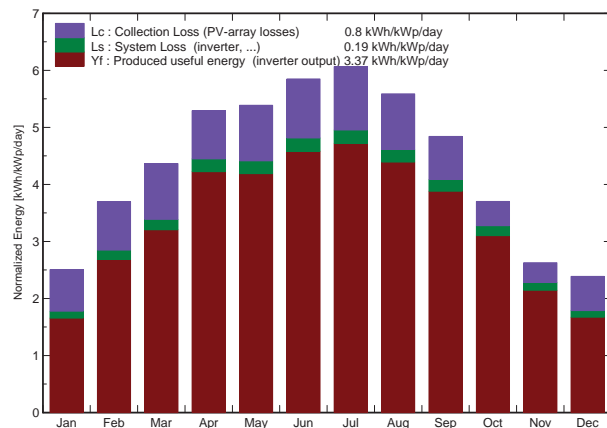
Grid-Connected System: Main results

Project : Peterborough DPW
Simulation variant : TERRASmart T25 A0 YL300 AE 333_060513

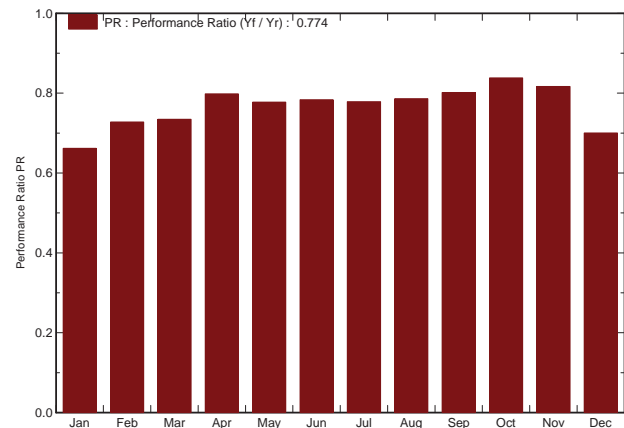
Main system parameters	System type	Grid-Connected	
PV Field Orientation	Sheds disposition, tilt	25 deg	azimuth 0 deg
PV modules	Model	YL300P-35b BSS01	Pnom 300 Wp
PV Array	Nb. of modules	3146	Pnom total 944 kWp
Inverter	Model	Solaron 333 BSS01	Pnom 333 kW ac
Inverter pack	Nb. of units	2.0	Pnom total 666 kW ac
User's needs	Unlimited load (grid)		

Main simulation results
System Production **Produced Energy 1162 MWh/year** Specific prod. 1231 kWh/kWp/year
Performance Ratio PR 77.4 %

Normalized productions (per installed kWp): Nominal power 944 kWp



Performance Ratio PR



TERRASmart T25 A0 YL300 AE 333_060513

Balances and main results

	GlobHor	T Amb	GlobInc	GlobEff	EArray	E_Grid	EffArrR	EffSysR
	kWh/m2	oC	kWh/m2	kWh/m2	MWh	MWh	%	%
January	49.4	-5.81	77.7	72.4	52.0	48.5	10.92	10.18
February	76.5	-5.25	103.5	97.8	75.3	71.1	11.86	11.19
March	112.0	1.62	135.3	128.6	99.1	93.8	11.94	11.30
April	144.7	7.67	158.7	150.9	125.9	119.6	12.93	12.28
May	163.9	14.29	167.0	158.4	129.1	122.6	12.60	11.96
June	177.9	18.39	175.5	166.3	136.3	129.7	12.66	12.05
July	186.4	21.81	188.0	178.6	144.9	138.1	12.57	11.97
August	163.0	19.63	173.2	164.6	135.0	128.5	12.70	12.09
September	123.0	15.72	145.3	138.4	115.7	109.9	12.98	12.33
October	86.5	8.70	114.8	109.0	95.9	90.8	13.62	12.90
November	54.0	2.52	78.8	73.7	64.6	60.7	13.37	12.56
December	47.2	-4.75	74.0	67.7	52.4	48.9	11.53	10.77
Year	1384.6	7.95	1591.7	1506.3	1226.3	1162.2	12.56	11.90

Legends:	GlobHor	Horizontal global irradiation	EArray	Effective energy at the output of the array
	T Amb	Ambient Temperature	E_Grid	Energy injected into grid
	GlobInc	Global incident in coll. plane	EffArrR	Effic. Eout array / rough area
	GlobEff	Effective Global, corr. for IAM and shadings	EffSysR	Effic. Eout system / rough area

Grid-Connected System: Loss diagram

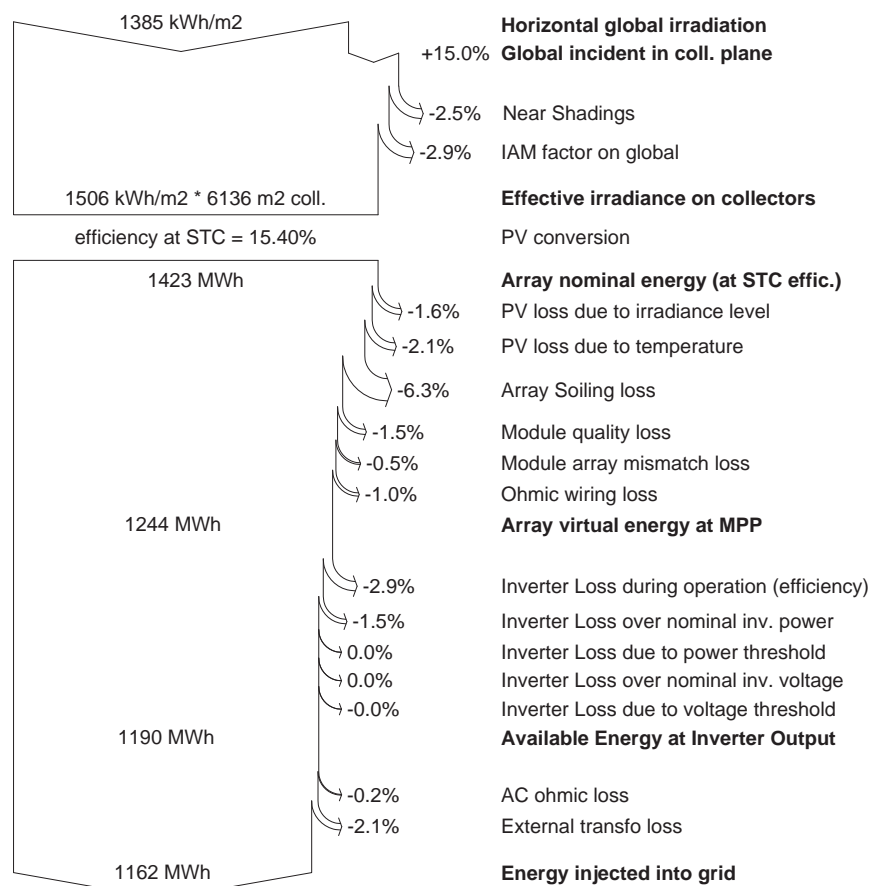
Project : Peterborough DPW

Simulation variant : TERRASMART T25 A0 YL300 AE 333_060513

Main system parameters

PV Field Orientation	System type	Grid-Connected		
PV modules	Sheds disposition, tilt	25 deg	azimuth	0 deg
PV Array	Model	YL300P-35b BSS01	Pnom	300 Wp
Inverter	Nb. of modules	3146	Pnom total	944 kWp
Inverter pack	Model	Solaron 333 BSS01	Pnom	333 kW ac
User's needs	Nb. of units	2.0	Pnom total	666 kW ac
	Unlimited load (grid)			

Loss diagram over the whole year



Peterborough WWTF PV Project - 12 X 24 Report (MWh)																									
Total Annual Production for Each Hour of Every Month (Summer Peak Hours Highlighted)																									
Corrected for Daylight Savings Time																									
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	Total
Jan	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	0.19	2.83	6.13	8.10	9.33	8.70	7.04	4.77	2.27	0.12	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	49
Feb	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.03	1.54	5.31	8.68	10.21	10.98	11.41	10.33	7.55	4.58	1.38	-0.03	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	71
Mar	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	0.02	1.44	5.27	8.98	11.31	12.98	13.52	12.35	11.48	8.90	5.89	2.37	0.26	-0.06	-0.06	-0.06	-0.06	-0.06	94
Apr	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	0.15	2.53	6.83	10.86	14.07	15.24	14.71	14.86	14.28	11.92	9.26	4.79	1.07	-0.03	-0.06	-0.06	-0.06	-0.06	120
May	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	1.30	4.28	7.81	11.88	13.29	14.07	13.83	14.17	13.00	12.58	9.48	5.69	2.00	0.22	-0.06	-0.06	-0.06	-0.06	123
Jun	-0.06	-0.06	-0.06	-0.06	-0.06	0.09	1.03	4.26	7.93	10.92	13.85	15.37	15.65	15.07	14.12	12.94	9.76	6.39	2.77	0.54	-0.06	-0.06	-0.06	-0.06	130
Jul	-0.06	-0.06	-0.06	-0.06	-0.06	-0.02	0.79	3.60	7.65	11.00	13.75	15.89	17.38	16.99	16.43	13.86	11.41	6.90	2.92	0.56	-0.06	-0.06	-0.06	-0.06	139
Aug	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	0.29	3.02	7.54	11.21	13.95	15.83	16.48	15.94	15.13	12.55	9.65	5.90	1.91	0.13	-0.06	-0.06	-0.06	-0.06	129
Sep	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	-0.01	1.86	5.51	9.79	13.57	14.22	15.39	14.46	13.65	11.26	7.38	3.42	0.39	-0.06	-0.06	-0.06	-0.06	-0.06	110
Oct	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	0.79	4.63	8.95	12.65	12.77	13.22	13.83	10.85	8.36	4.79	1.02	-0.05	-0.06	-0.06	-0.06	-0.06	-0.06	91
Nov	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	-0.03	1.58	4.88	7.73	10.51	10.74	9.84	8.62	5.20	2.28	0.29	-0.02	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	61
Dec	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	0.49	3.28	6.70	8.95	9.35	8.80	6.99	4.14	1.23	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06	49
Average	-1	-1	-1	-1	-1	0	3	26	69	113	144	157	159	151	131	103	69	36	11	1	-1	-1	-1	-1	1166.3

Peterborough WWTF PV Project - 12 X 24 Report (MWh)																									
Average Production for Each Hour of Every Month (Summer Peak Hours Highlighted)																									
Corrected for Daylight Savings Time																									
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	Total
Jan	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.09	0.20	0.26	0.30	0.28	0.23	0.15	0.07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.6
Feb	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.06	0.19	0.31	0.36	0.39	0.41	0.37	0.27	0.16	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.5
Mar	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.17	0.29	0.36	0.42	0.44	0.40	0.37	0.29	0.19	0.08	0.01	0.00	0.00	0.00	0.00	0.00	3.0
Apr	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.08	0.23	0.36	0.47	0.51	0.49	0.50	0.48	0.40	0.31	0.16	0.04	0.00	0.00	0.00	0.00	0.00	4.0
May	0.00	0.00	0.00	0.00	0.00	0.00	0.04	0.14	0.25	0.38	0.43	0.45	0.45	0.46	0.42	0.41	0.31	0.18	0.06	0.01	0.00	0.00	0.00	0.00	4.0
Jun	0.00	0.00	0.00	0.00	0.00	0.00	0.03	0.14	0.26	0.36	0.46	0.51	0.52	0.50	0.47	0.43	0.33	0.21	0.09	0.02	0.00	0.00	0.00	0.00	4.3
Jul	0.00	0.00	0.00	0.00	0.00	0.00	0.03	0.12	0.25	0.35	0.44	0.51	0.56	0.55	0.53	0.45	0.37	0.22	0.09	0.02	0.00	0.00	0.00	0.00	4.5
Aug	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.10	0.24	0.36	0.45	0.51	0.53	0.51	0.49	0.40	0.31	0.19	0.06	0.00	0.00	0.00	0.00	0.00	4.2
Sep	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.06	0.18	0.33	0.45	0.47	0.51	0.48	0.46	0.38	0.25	0.11	0.01	0.00	0.00	0.00	0.00	0.00	3.7
Oct	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.03	0.15	0.29	0.41	0.41	0.43	0.45	0.35	0.27	0.15	0.03	0.00	0.00	0.00	0.00	0.00	0.00	2.9
Nov	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.16	0.26	0.35	0.36	0.33	0.29	0.17	0.08	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.0
Dec	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	0.11	0.22	0.29	0.30	0.28	0.23	0.13	0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.6
Average	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.4	0.4	0.4	0.4	0.4	0.3	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	

Production Mo for Grid-Tied PV Systems

Production modeling meets multiple needs. Integrators seek to optimize PV system designs or to provide production guarantees; investors look to verify the right return on investment; operators need performance expectations to compare to measured performance.

All sectors of the maturing solar industry demand accurate production estimates, which require a clear understanding of how the estimates are produced and an ability to interpret the results. In this article we provide an overview of production-modeling theory and review available production-modeling tools. We compare the tools' performance to each other and to real systems, and provide a summary of the key uses of production modeling in PV projects.

At the most basic level, production modeling comes down to two questions:

1. How much sunlight falls on an array?
2. How much power can a system produce with that sunlight?

Answering these questions requires location-specific parameters, such as shading and weather data; educated assumptions about system derating due to soiling, module mismatch, system availability; and complex algorithms to model available radiation as well as module and inverter performance.

HOW MUCH SUN?

A PV system's geographical location, surroundings and configuration determine the amount of sunlight that falls on the modules. Where a system is located geographically determines how much sunlight is available; the surroundings dictate the amount of available sunlight that is blocked before reaching the array; and the array configuration determines how efficient the system is at exposing the modules to sunlight.

Meteorological data. The first factor in determining how much sunlight falls on an array is meteorological data that accurately represent the weather at a system's location. Meteorological data typically include solar radiation (global horizontal, direct beam and horizontal diffuse), temperature, cloud cover, wind speed and direction, along with other meteorological elements. The data are based on ground or satellite measurements and in some instances are modeled rather than measured.

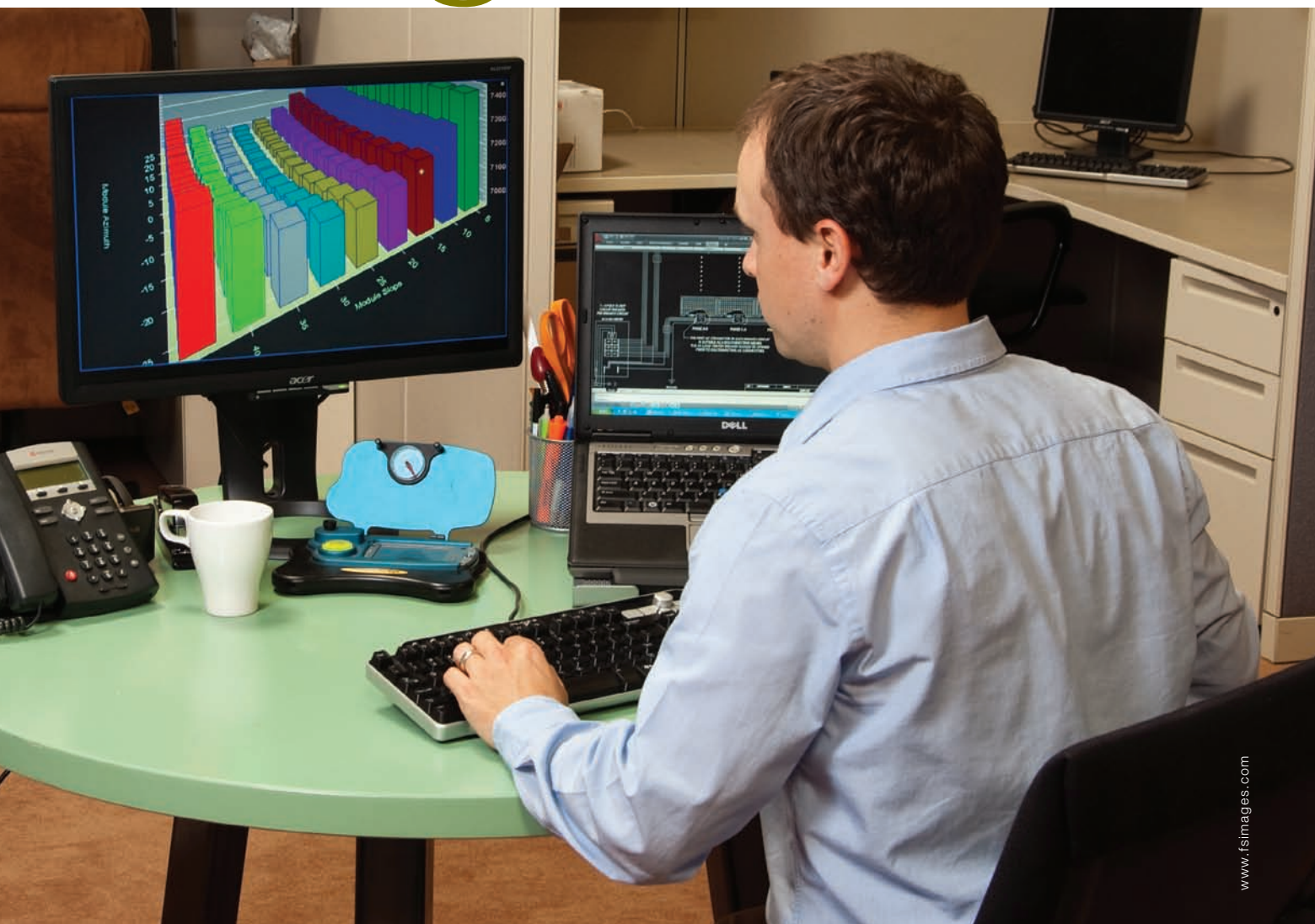
Typically a large amount of analysis is involved in taking raw data and producing a data set suitable for use. Meteorological data are typically measured by government agencies and utilized by a variety of organizations that make the data available in formats suitable for use in production-modeling tools. These organizations include the National Renewable Energy Laboratory (NREL) and NASA, which provide the information free of charge, and also organizations such as Meteonorm and 3Tier, which provide the data for a fee.

The most common sources of data for US solar projects are the Typical Meteorological Year (TMY) files published by NREL and based on analysis of the National Solar Radiation Data Base (NSRDB). TMY data comprise sets of hourly values of solar radiation and meteorological elements representing a single year. Individual months in the data record are examined, and the most "typical" are selected and concatenated to form a year of data. Due to variations in weather patterns, these data are better indicators of long-term performance rather than performance for a given month or year. According to the online document "Cautions for Interpreting the Results" that NREL publishes along with its PVWatts tool (see Resources), these data may vary as much as $\pm 10\%$ on an annual basis and $\pm 30\%$ on a monthly basis.

The first TMY data set was published in 1978 for 248 locations throughout the US. The data set was updated in 1994 from the 1961–1990 NSRDB to create a set of TMY files, called TMY2, for 237 US locations. A subsequent 2007 update utilized an expanded NSRDB from 1999–2005 to create TMY3, which covers 1,020 locations across the US. TMY3 data are categorized into three classes that reflect the certainty and completeness of the data, with Class I being the most certain, Class II less certain and Class III being incomplete data. TMY, TMY2 and TMY3 present changes in reference time, format, data content and units from set to set. The data sets are incompatible with each other, but conversion tools are available. The TMY2 and TMY3 data sets are either utilized by or can be imported into all of the major PV performance-modeling tools used in the US.

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By Tarn Yates and Bradley Hibberd



Radiation models. Typical weather data include three solar radiation values representing radiation incident on a horizontal surface: direct beam, horizontal diffuse and global horizontal radiation. Direct beam radiation is light that travels in a straight line from the sun, whereas diffuse radiation is light that is scattered by the atmosphere or by clouds. In theory, global horizontal radiation is the sum of the direct beam and the horizontal diffuse radiation. However, this is not always the case due to measurement inaccuracies and modeling techniques.

Meteorological data indicate how much radiation falls on a horizontal surface, but how much falls on an array? While occasionally installed flat, PV systems usually have a

tilt and an azimuth or employ single- or dual-axis trackers. A mathematical model is needed to translate horizontal radiation values into *plane-of-array* (POA) irradiance. The accuracy of a radiation model is affected by the weather at the system location and by the quality of the weather data.

Numerous models are used to make this translation, including the Perez et al., Reindel, Hay and Davies, and Isotropic Sky models. The Perez et al. model is the most complex. A test performed in Albuquerque, New Mexico, by Sandia showed that Perez et al. model predictions are the closest to measured data. This is documented in the Sandia article "Comparison of PV System Performance-Model Predictions

with Measured PV System Performance” (see Resources).

In general, radiation models treat the direct beam component the same way. Using the latitude and longitude of the system location as well as the time of day, it is possible to calculate the sun’s position in the sky. Once this is known, the translation of direct beam radiation to POA radiation is a relatively simple geometric calculation.

Where the models differ is in the treatment of diffuse radiation. The Isotropic Sky model assumes diffuse radiation is emitted equally from every portion of the sky. More advanced models take into account the fact that diffuse radiation is more intense at the horizon and in the circum-solar region, the area directly surrounding the sun. They may also consider variations in intensity based on the altitude angle of a section of sky, the clearness and brightness of the sky, and the air mass. Refer to *Solar Radiation and Daylight Models* for a history and review of radiation models (see Resources).

An additional component of radiation is the radiation reflected by the ground or by the roof or surfaces associated with the ground or roof. The reflected radiation is a function of the *albedo* of the surface, a term that describes the reflective qualities of a surface. The amount of reflected radiation is also a function of the angle of the array; an array at zero degrees will receive no reflected radiation. The amount of radiation received from reflection will increase with increasing tilt angle. Albedo varies with the surface and can change throughout the year with weather conditions such as snow. Modeling programs give you a variety of methods to account

“PV production models are really quite simple. Making an accurate model is straightforward. The difficult part is getting the right input assumptions that drive the model—the most critical of these, of course, being insolation.”

—Joe Song,
director of engineering,
SunEdison

for this. For example, both PVsyst and PV*SOL allow you to define monthly values for the albedo, whereas the Solar Advisor Model (SAM) changes the albedo if the weather data indicate snow.

Shading. Simply translating horizontal radiation into POA radiation does not tell the whole story. Depending on the PV system location and configuration, large

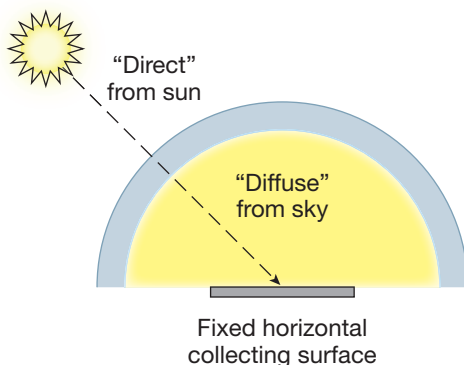
distant objects, close obstructions and the system itself may block some of the available sunlight. The complexity of the performance-modeling tool dictates whether these types of shading are treated separately or grouped together. In the latter case, shading is accounted for by a single derate factor.

Using a single derate factor for shading assumes that the system experiences the same losses due to shade for every hour of the year. In addition, most production-modeling tools assume that the effects of shade are linear. That is, if 10% of the array is shaded, then you lose 10% of the expected energy production. This is not an accurate model, because shading just one cell in a module can disproportionately impact the whole module, the string or even the entire array.

Accurately defining shading is very difficult. It is not possible to simply go out to a proposed project location, look around and determine a shading derate factor. This is where tools like the Solmetric SunEye and Solar Pathfinder are useful, because these tools quantify shading factors that can be used in many of the production-modeling tools. Both Solmetric and Solar Pathfinder have their own production software that is designed to interact with data collected using their shade survey tools. (For more information on this topic, see “Solar Site Evaluation: Tools and Techniques to Quantify & Optimize Production,” December/January 2009, *SolarPro* magazine.)

Soiling. An additional factor that decreases the available sunlight is soiling caused by the accumulation of particulates, such as dust, snow, pollutants and bird droppings. The power lost due to soiling is affected by the tilt of the array, the quantity and seasonal variability of rain and snowfall, the system’s cleaning schedule and any site-specific conditions, such as the proximity to a major roadway or a commercial operation that creates dust. Most tools allow you to enter an annual soiling derate factor only. This is not sufficient if the value of power is determined by the period of time in which the power is produced. For example, estimates for the production losses due to soiling in California can be around 1% in winter and at least as high as 10% in late summer for a system that is not washed—a significant loss during a prime production period that an annual soiling factor would not accurately take into account. CONTINUED ON PAGE 34

mollyohalloran.com



Global horizontal radiation According to NREL’s “Glossary of Solar Radiation Resource Terms,” while total solar radiation is the sum of direct, diffuse and ground-reflected radiation, the amount of radiation reflected off of the ground is usually insignificant. As a result, global horizontal radiation is generally referred to as the sum of direct and diffuse radiation.

HOW MUCH POWER?

The second step in production modeling is determining how effective a PV system is at converting the sunlight incident on an array into usable power.

PV PERFORMANCE MODELS

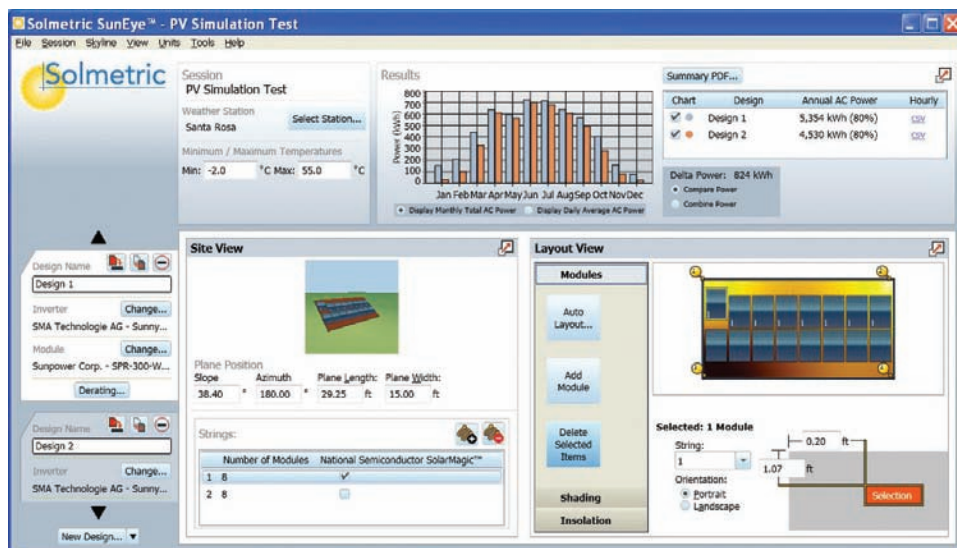
Several models have been created to predict the power output of a solar cell, module or array. Both complex and simple models exist. Here we describe some of the more relevant models.

Sandia performance model. In 2004, Sandia National Laboratories published “Photovoltaic Array Performance Model,” which outlines the Sandia array performance model (see Resources). This is one of the more robust production models. The Sandia performance model is based on a series of empirically derived formulas that define five points on the IV curve of a PV cell. These five points can be used to produce an approximation of the actual curve. The model requires approximately 30 coefficients that are measured on a two-axis tracker at the Sandia National Labs in Albuquerque, New Mexico.

The coefficients used in the Sandia model take into consideration module construction and racking technique, solar spectral influences, angle of incidence effects and the irradiance dependence of electrical characteristics such as the temperature coefficients of power, voltage and current. Tests documented in “Comparison of Photovoltaic Module Performance Measurements” show that the model can predict power output to within 1% of measured power (see Resources).

The Sandia performance model is an option in both Solar Advisor Model (SAM) and PV-DesignPro. One of the challenges associated with this model is that the modules must undergo testing at the Sandia labs to be included. Unfortunately, this means that the Sandia database of modules often does not include recently released modules. This issue should soon be alleviated, as Sandia entered an agreement to have commercially available modules tested by TÜV Rheinland Photovoltaic Testing Laboratory at its facilities in Tempe, Arizona.

Single-diode performance model. The single-diode model assumes that the behavior of a PV cell can be simulated by an equivalent circuit consisting of a current source, a diode and two or three resistors, as shown in Figure 1. The current source and diode represent the ideal behavior of a solar cell, and the series and shunt resistors are used to model



Quantifying shade Solmetric’s recently released PV Designer software tool allows you to drag icons representing data collected by its SunEye tool onto a visual representation of a roof surface.

real-world losses, such as current leaks and resistance between the metallic contacts and the semiconductor.

Using circuit theory, you can define equations that describe the current and voltage characteristics of the equivalent circuit. Unknown variables can be determined by evaluating the equations at conditions such as those specified on the manufacturers’ spec sheet for open-circuit voltage and short-circuit current. The single-diode performance model is the basis of both the model used in PVsyst and the CEC model that is an option in SAM.

PVFORM model. The performance model that PVWatts uses is a simplified version of a model developed at Sandia called PVFORM. This model uses the POA irradiance, ambient temperature and wind speed to calculate the operating temperature of a solar cell. It then calculates the power output of the system by adjusting the STC capacity rating of the array based on the POA irradiance and the cell temperature. As implemented in PVWatts, this model assumes that the temperature coefficient of power for a PV module is $-0.5\%/^{\circ}\text{C}$. This is a reasonable approximation for crystalline silicon modules that have temperature coefficients in the -0.55 to $-0.40\%/^{\circ}\text{C}$ range. However, it is not appropriate for other technologies, such as thin film, that typically have temperature coefficients in the -0.26 to $-0.20\%/^{\circ}\text{C}$ range.

DC DERATE FACTORS

The major factors that determine the amount of dc power produced for a given level of illumination are the efficiency of the technology, the temperature of the module cells and the technology’s response to changes in temperature. Other factors that should be considered for accurate production

modeling are the accuracy of the nameplate rating of the module, losses due to module mismatch, voltage drop across the diodes and connections in the modules, the resistance of the dc wiring, module degradation, the inverter's accuracy at tracking the maximum power point of the array and the angle of incidence of the sunlight.

Once the theoretical power output of the array has been calculated, a series of derate factors must be applied to arrive at the actual power that will be delivered to the inverter. Following are some of the major factors.

Module nameplate rating. Module manufacturers assign a range of accuracy to the nameplate rating of their modules, such as $\pm 5\%$. This means that a module rated at 200 W may have a power output of only 190 W. Unless the tolerance is -0% , many modules do not have an STC rating as high as that specified. A conservative value to use for this factor is one that assumes that all of the modules have a rating at the low end of the tolerance.

DC wiring losses. Most integrators have standards for acceptable voltage drop that provide a good starting point for determining this number. It is common for a wiring loss factor to be calculated using the current and voltage at the maximum power point at STC conditions, as specified on the manufacturer's data sheet. Less rigorous tools take this single factor and apply it over all operating conditions. This practice neglects the fact that the current and voltage are rarely equal to the values specified on the spec sheet. More advanced programs (such as PVsyst, PV*SOL and PV-DesignPro) ask you to specify the size of conductors and length of the wire run, or specifically ask for the losses at STC. They then calculate the wiring losses at other operating conditions.

Module mismatch. This derate factor accounts for the fact that the current and voltage characteristics of every module are not identical. Although the MPPT in the inverter keeps the array at its maximum power point, each individual module does not operate at its maximum power point. A loss of 2% is a typical estimate for module mismatch. (Note that this factor is not relevant when using microinverters.)

MPPT efficiency. According to "Performance Model for Grid-Connected Photovoltaic Inverters" (see Resources), most grid-tied PV inverters are between 98% and 100% efficient at capturing the maximum available power from a PV array.

Degradation. If you are modeling future production, the degradation of power over time must be considered. A standard value for module degradation is 1% per year. Recent

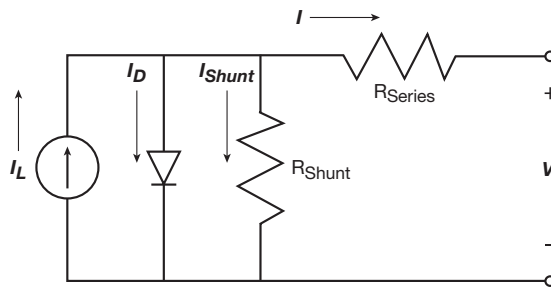


Figure 1 This diagram shows the solar cell equivalent circuit used in the single-diode performance model. The current from the current source, I_L , is directly proportional to the intensity of the available light and the corresponding photoelectric effect.

warranties for crystalline modules, such as the 85% power guarantee after 25 years offered with Suntech's Reliathon module, indicate that manufacturers expect the value to be less. Additionally, "Comparison of Degradation Rates of Individual Modules Held at Maximum Power" (see Resources) suggests that 0.5% per year is a better rule of thumb for crystalline modules, but notes that it should be higher than 1% for many thin-film modules.

AC DERATE FACTORS

Unfortunately, the conversion of dc power delivered to the inverter into ac power at the point of interconnection is not a lossless process. The inverter is the major factor in this stage, but it is also important to consider losses due to wiring, transformers and system downtime.

AC wiring losses. As with dc wiring, the losses due to resistance in ac wiring vary with the amount of current. In the case of ac current, loss factor calculations typically assume full power output from the inverter. This occurs for only a portion of the inverter's operating time.

Transformer losses. When a transformer that is not included as part of the inverter is required, it is necessary to account for its losses. While many transformers are more than 98% efficient, it is worth verifying the transformer's efficiency.

System downtime. Every PV system experiences downtime at some point. This can be due to the failure of an inverter or a short in a single string. The severity and duration of the downtime can be mitigated by diligent maintenance, monitoring and rapid response.

INVERTER PERFORMANCE MODELS

According to the authors of Sandia's "Performance Model for Grid-Connected Photovoltaic Inverters" (see Resources), "Frequently in modeling PV system energy production, inverter efficiency is assumed to be a constant value, which is the same as assuming that inverter efficiency is linear over its operating range, which is clearly not the case." In reality, the inverter efficiency depends on both the loading of the inverter and on the input voltage of the array. This is illustrated in Figure 2 (p. 36), which shows a typical inverter efficiency graph available through the CEC. A similar graph is available for every inverter that is approved for incentives in California. An accurate inverter model should account for any power shaving that may occur due to overloading or inverter shutdown due to the dc voltage being out of range. The power consumption of the

inverter under standby and operating conditions is also a factor in total power production.

Sandia performance model for grid-connected PV inverters. The Sandia inverter model is similar to the Sandia module model in that it is based on empirically derived equations. It considers the ac power output of an inverter to be a function of the dc input power and voltage. Several coefficients are used to define this relationship. It is possible to approximate a version of the inverter model with parameters usually available on a manufacturer's spec sheet. Field and laboratory testing enable more refined versions of the inverter model. A benefit of this model is that it is compatible with the parameters recorded as part of the CEC testing process, and therefore the associated database is kept up-to-date. A Sandia study showed this model to be accurate to within 0.2% when compared to measured results. The Sandia inverter model is available in the system production-modeling tool SAM.

Other inverter models. The single-point efficiency model is utilized in PVWatts and is also an option in SAM. This model specifies a conversion efficiency that is used for all operating conditions. In PVsyst and PV*SOL, inverters are defined by the manufacturers' spec sheet values, such as the maximum power rating, the MPPT voltage range, the threshold power and the inverter's efficiency at various levels of loading. These programs use the efficiency inputs to define a curve that is used in simulations. Although not a perfect correlation, input values for defining inverter efficiency curves can be pulled from the online results of the CEC inverter tests at Go Solar California, as illustrated in Figure 2.

PHOTOVOLTAIC PRODUCTION-MODELING TOOLS

While it is beyond the scope of this article to compare all of the available production-modeling tools, we review the major software packages currently utilized by researchers, integrators and project developers in North America: PVWatts, Solar Advisor Model, PV-DesignPro, PV*SOL and PVsyst.

These production-modeling tools, along with five others, are surveyed in the companion table, "2010 Production-Modeling Tools," on pages 40–43. This table does not include estimators used by various incentive or rebate programs and tools that are primarily intended to generate sales quotes and proposals. Some of the entries in this table are adopted from a table developed by Geoffrey Klise and Joshua Stein for their article "Models Used to Assess the Performance of Photovoltaic Systems" (see Resources.)

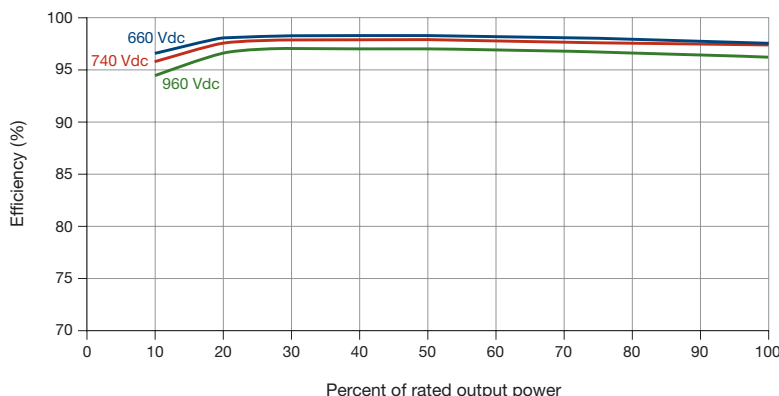


Figure 2 This graph is typical of the performance test results available for all CEC-eligible inverters, showing, in this case, how the efficiency of an AE Solaron 333 is a function of inverter loading and dc input voltage.

PVWATTS

PVWatts was developed by NREL and has long been the default production-modeling tool of the US PV industry. Its strength lies in its simplicity. You can make a reasonable estimate of a system's production by selecting the location from a US map, entering the system size in dc watts and specifying the array tilt and azimuth. You can also select single- or dual-axis tracking options. By default the program uses a single conservative derate factor. This value is based on assumptions for variables such as the inverter efficiency, ac and dc wiring losses, and soiling. You can easily revise these assumptions to recalculate the derate factor.

PVWatts provides estimates of the monthly and annual values for the ac energy production and average solar radiation per day, plus a rough calculation of the value of the energy produced based on local energy rates. These values are often reasonable estimates, but PVWatts lacks the level of control and specificity of results that can be found in other tools.

Version 1. PVWatts v. 1 presents a simple map of the US from which to choose the state where the project is located. You then chose the TMY2 data location that is closest to the project site (in some instances the closest data location may not be in the same state). A feature specific to v. 1 is that it outputs an 8,760 report—an hour-by-hour report of energy production for the entire year—in text format.

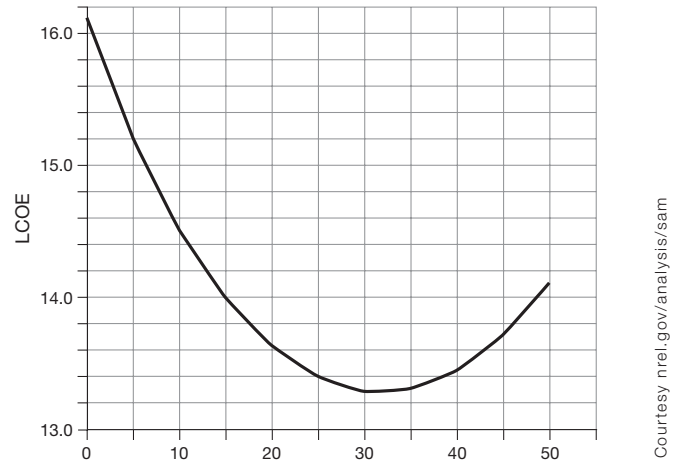
Version 2. PVWatts v. 2 provides a map of the US that is divided into 40-by-40 km grid areas. The program then combines data from the closest TMY2 data location with monthly weather data that are specific to the grid area that you select. This more accurately reflects local weather conditions and accounts for distances from the TMY2 data locations. The v. 2 map is searchable by zip code or by latitude and longitude. A beta version of a new PVWatts v. 2 map viewer was recently released. This new interface allows you to quickly see the annual and monthly irradiance

specific to each grid cell. It is also easier to navigate and more attractive.

SOLAR ADVISOR MODEL (SAM)

SAM was produced by NREL in conjunction with Sandia through the US Department of Energy's Solar Energy Technologies Program. It is a step up from PVWatts in the level of control available. SAM provides a wide range of options for estimating PV module production, including the Sandia PV array performance model, the CEC performance model and the PVWatts performance model. The Sandia inverter performance model is used to simulate inverter performance. You can select modules and inverters from databases so that the specific characteristics of the system components can be used in the simulations. In cases where components are not in the databases, simple efficiency models can represent their performance. SAM uses two composite derate factors, pre-inverter and post-inverter, to account for system losses. A 12-month-by-24-hour matrix is used to define the percent of shading for every hour of every month of the year.

In addition to its production-modeling capabilities, SAM puts an emphasis on analyzing the financials involved in PV project development. The analysis focuses on the US market



Parametric analysis The results from the parametric analysis optimization tool in SAM show that the tilt resulting in the minimum levelized cost of energy (LCOE) is 32.5° with an LCOE of 19.15 ¢/kWh. This graph assumes a cash purchase, using the default system cost and financial information provided in SAM. The system modeled consists of 1,190 Sharp ND-216U1F modules with a due south azimuth connected to a SMA Sunny Central 250U inverter in San Francisco, CA.

and includes tax credits, depreciation, and capacity- and production-based incentives. Detailed cash flow models are available for residential, commercial and utility-scale projects that can be used to calculate parameters such as the levelized cost of energy (LCOE). SAM provides a method for entering utility rate schedules, including time of use (TOU) schedules, to accurately represent the varying value of electricity.

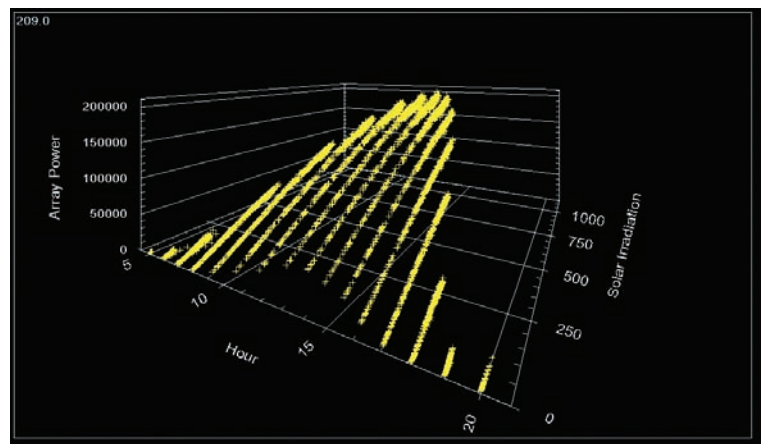
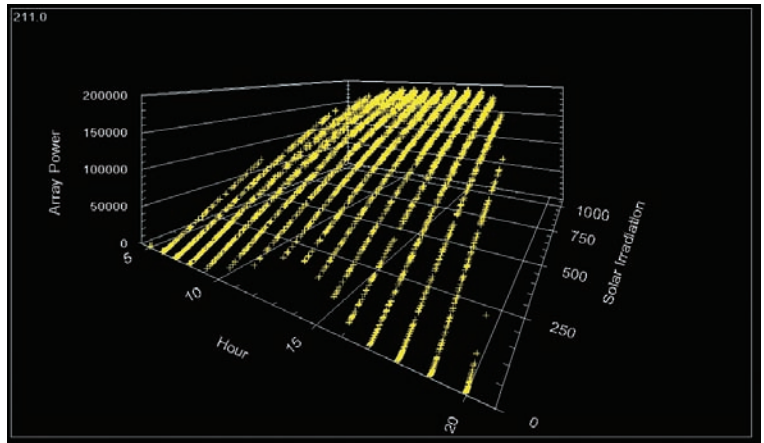
SAM contains a suite of analysis tools that includes parametric, optimization, sensitivity and statistical tools. These tools give you insight into how changes in system variables (including tilt, azimuth, system capacity or component cost) impact output metrics such as annual production or LCOE. The parametric and optimization tools run numerous iterations of the production simulation, stepping through a range of values that you can define for one or more system variables. The optimization tool maximizes or minimizes a specified output metric, whereas the parametric tool provides a broader view of the relationship between system variables and output metrics.

Two interesting new features were added to the program with the release of the latest version in October 2009. A scripting language called SAMUL has been developed for SAM that is similar to the VBA language available in Microsoft Excel. This allows you to control many of the program functions through code, and it facilitates the automation of repetitive tasks. In addition, the program now generates source code in Excel/VBA, C and MATLAB formats so that the core simulation engine can be accessed separately from the user interface.

PV-DESIGNPRO

PV-DesignPro was developed by Maui Solar Energy Software. The program is similar to SAM in that you define system configuration and derate factors. PV-DesignPro utilizes the Sandia PV array performance model and provides module and inverter databases from which to choose system components. The program accounts for shading by means of a horizon profile that you define by specifying the azimuth and altitude angle as well as the opacity of the obstruction. You also have the ability to define the size and length of wire runs, as well as the efficiency of the inverter's MPPT. All other system losses are accounted for in overall current and voltage derate factors.

One of PV-DesignPro's strengths is the wealth of information that it supplies. At every step in the process the program attempts to provide as much insight as possible into the variables that affect energy production. Once you select a system location, for example, the program produces charts showing detailed irradiance, temperature and wind data for



Courtesy maui-solarsoftware.com

PV-DesignPro scatter plots These plots, with the hour of the day and the solar irradiance on the horizontal plane and the array power in dc watts on the vertical axis, show the difference in production for a horizontal single-axis (north-south) tracker and a fixed system with a tilt of 37° and an azimuth of 0° (true south) in San Francisco, CA. Each figure shows 8,760 data points, one for every hour of the year. (System specifications: 1,376 Mitsubishi PV-UD185MF5 modules; one Xantrex PV225 inverter.)

every day of the year. When defining system capacity, graphs show typical IV curves and the max power of the array at cell temperatures from 25°C to 50°C. Once you have run a simulation, you can create scatter plots containing data on system variables for every hour of the year. These scatter plots can be used to visualize and learn about system behavior or to inform design decisions.

PV-DesignPro also performs parametric analyses and produces graphs that illustrate how changes in system variables influence production and financial parameters. This function can help you minimize or maximize important variables such as kWh production or the cost of a utility bill. The software also includes tools to produce detailed load and TOU profiles. These can be used to

CONTINUED ON PAGE 44

2010 Production Modeling Tools ¹

Software Program	Basics			Weather Data Source	Irradiance Model
	Developer	Cost	Web-Based or Application		
HOMER	HOMER ENERGY, originally developed by NREL	free	application	user provides hourly average global solar radiation on the horizontal surface (kW/m ²), monthly average global solar radiation on the horizontal surface (kWh/m ² /day), or monthly average clearness index	Hay and Davies model
Polysun	Vela Solaris	Light \$159 Pro \$489	application	Meteotest	unknown
PV Designer	Solmetric	\$400/yr	application	various weather sources including TMY2 and TMY3 data; outside the US, the same weather sources as Energy Plus	Perez et al. model
PV-DesignPro	Maui Solar Energy Software with Sandia	\$259	application	TMY2, TMY3, Meteonorm, Global Solar Irradiation Database	Perez et al. model (default), HDKR model (option)
PV F-Chart	F-Chart Software with University of Wisconsin	\$400	application	TMY2, TMY3, weather data can be added	Isotropic Sky model
PV*SOL	Valentin Software	\$698 ²	application	MeteoSyn, Meteonorm, SWERA, PVGIS, NASA SSE	Hay and Davies model
PVsyst	University of Geneva	1st license \$984, additional \$197	application	TMY2, TMY3, Meteonorm, ISM-EMPA, Helioclim-1 and -3, NASA-SSE, WRDC, PVGIS-ESRA and RETScreen; user can import custom data in a CSV file	Hay and Davies model (default), Perez et al. model (option)
PVWatts v. 1	NREL	free	Web	in the US—TMY2 data; 239 options outside the US—TMY data from the Solar and Wind Energy Resource Assessment Programme, the International Weather for Energy Calculations (V1.1), and the Canadian Weather for Energy Calculations	Perez et al. model
PVWatts v. 2	NREL	free	Web	combination of TMY2 data with monthly weather data from Real-Time Nephanalysis (RTNEPH) database (cloud cover), Canadian Center for Remote Sensing (albedo), National Climatic Data Center (daily maximum dry bulb temperatures) and RDI/FT Energy (1999 residential electric rates)	Perez et al. model
RetScreen	Natural Resources Canada	free	application	combination of weather data collected from 4,720 sites from 20 different sources with data from 1961–1990 & NASA-SSE	Isotropic Sky model
Solar Advisor Model (SAM)	NREL	free	application	TMY2, TMY3, EPW, Meteronorm	Perez et al. model (default); Isotropic Sky Model, Hay and Davies model, Reindl model (options); total and beam (default), beam and diffuse (option)

Notes:

¹ Some entries in this table adopted from Klise and Stein (2009). ² Does not include expert version to be released in 2010.

³ Shading derate is from SunEye readings. Inverter efficiency derate is from an equipment database.

⁴ User enters array operating temperature, reference efficiency, temperature coefficient and array area.

Modeling					
Production-Estimating Model: Module	Production-Estimating Model: Inverter	Simulation Frequency	Tilt	Orientation	Derate Factors
linear irradiance model with temperature correction	single efficiency derate factor	hourly	manual input	manual input	derate factors not categorized, all losses except for single percentage for inverter efficiency are covered by “miscellaneous losses”
empirical model of module performance, dependent on three MPPT power ratings at different irradiance values and the module temperature coefficient	unknown	hourly	manual input	manual input	soiling, degradation, mismatch, wiring
proprietary model based on nominal power and operating temperature	single-weighted efficiency derate factor	hourly	manual input	manual input	PV module nameplate dc rating, inverter and transformer, mismatch, diodes and connections, dc wiring, ac wiring, soiling, system availability, shading, sun tracking, age ³
Sandia model	Sandia model	hourly	manual input	manual input	wiring, MPPT efficiency, array current derate factor, array voltage derate factor
function of efficiency and temperature	power tracking and power conversion efficiency factors	hourly	manual input	manual input	inverter conversion efficiency and power tracking efficiency
modeled using V and irradiance at STC, module efficiency curve and an incident angle modifier; linear or dynamic temperature model options	inverter profile and efficiency curve generated from measured data	hourly	manual input	manual input	mismatch, diodes, module quality, soiling, wiring, deviation from standard spectrum, module height above ground
Shockley's one-diode model for crystalline silicon; modified one-diode model for thin film	inverter profile and efficiency curve generated from measured data	hourly	manual input	manual input	field thermal loss, standard NOCT factor, Ohmic losses, module quality, mismatch, soiling (annual or monthly), IAM losses
simplified PVFORM	single efficiency derate factor	hourly	manual input	manual input	PV module nameplate dc rating, inverter and transformer, mismatch, diodes and connections, dc wiring, ac wiring, soiling, system availability, shading, sun tracking, age
simplified PVFORM	single efficiency derate factor	monthly	manual input	manual input	PV module nameplate dc rating, inverter and transformer, mismatch, diodes and connections, dc wiring, ac wiring, soiling, system availability, shading, sun tracking, age
Evan's average efficiency model	single efficiency derate factor	monthly	manual input	manual input	inverter efficiency, miscellaneous losses
Sandia model, CEC model, PVWatts model	single efficiency derate factor, Sandia Model for grid-connected inverters	hourly	manual input	manual input	mismatch, diodes and connections, dc wiring, soiling, sun tracking, ac wiring, transformer

2010 Production Modeling Tools

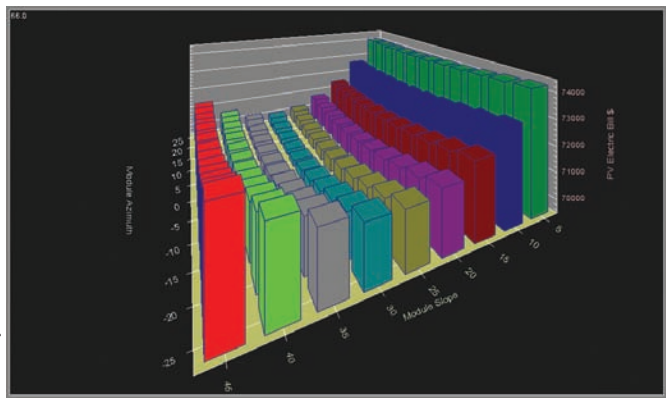
Software Program	Modeling			Output Data
	Technologies	Tracking	Shading	
HOMER	not technology specific ⁴	single axis (horizontal, daily adjustment), single axis (horizontal, weekly adjustment), single axis (horizontal monthly adjustment), single axis (horizontal, continuous adjustment), single axis (vertical, continuous adjustment), dual axis	not considered independently, could be incorporated into single derate factor	hourly ac production data
Polysun	cSi, aSi, CdTe, CIS, CIGS, HIT, μ c-Si, Ribbon (EFG)	single axis, dual axis	horizon profile may be defined or imported	unknown
PV Designer	cSi, aSi, CdTe, CIS	n/a	sub-module level shading, computed based on distance-weighted interpolation of readings taken from Solmetric SunEye	hourly ac energy production; daily and monthly ac energy production displayed graphically on screen
PV-DesignPro	cSi, aSi, CdTe, CIS, CPV, mj-CPV	single axis (horizontal axis EW), single axis (horizontal axis NS), single axis (vertical axis), single axis (NS axis parallel to Earth's axis), dual axis	horizon profile user-defined	hourly data available for meteorological data, PV array behavior (cell temp, module efficiency), energy production and more
PV F-Chart	not technology specific ⁴	flat-plate array, single-axis tracking (adjustable tilt/azimuth), dual-axis tracking, concentrating parabolic collector	not considered, could be incorporated into other derate factors	monthly average hourly values of ac energy
PV*SOL	cSi, aSi, CdTe, CIS, HIT, μ c-Si, Ribbon	single axis (vertical), dual axis	horizon profile user-defined or imported from shade survey tool, 3D modeling environment in Expert version	hourly energy production in one-week segments
PVsyst	cSi, HIT, CdTe, aSi, CIS, μ c-Si	single axis (horizontal axis EW), single axis (vertical axis), single axis (tilted axis), dual axis, dual axis (frame NS), dual axis (frame EW), tracking sun shields; ability to define parameters such as collector width, shade spacing and rotation limits	horizon profile can be user-defined or imported from a shade survey tool, 3D modeling environment, based on array configuration	hourly data available for meteorological data, PV array behavior (cell temp, wiring losses, etc.), energy production
PVWatts v. 1	cSi	single axis, dual axis	single derate factor	hourly ac energy production
PVWatts v. 2	cSi	single axis, dual axis	single derate factor	n/a
RetScreen	cSi, aSi, CdTe, CIS, spherical-Si	single axis, dual axis, azimuth	n/a	n/a
Solar Advisor Model (SAM)	cSi, aSi, CdTe, CIS, CPV, HIT	single axis (tilted NS axis), dual axis	12-month by 24-hour shade profile can be imported	hourly data available for meteorological data, PV array behavior (cell temp, wiring losses, etc.), energy production

Notes:

⁴ User enters array operating temperature, reference efficiency, temperature coefficient and array area. n/a = not available

Details			Component Database			
Financial Analyses	Ability to Export Data to Excel	Optimization	Module	Inverter	Update Method and Frequency	User Support & Documentation
cash-flow analysis considering energy costs, operating costs and calculation of LCOE	exported as a text file	sensitivity analysis and optimization capability	n/a	n/a	n/a	user manual provided with software
financial analysis including O&M costs, incentives, projected electricity costs, inflation and interest rates	yes	n/a	yes	yes	automatically checks for updates	user manual provided with software
n/a	yes	n/a	yes	yes	component data compiled from PVXchange database, updated approximately monthly	user manual provided with software
basic cash-flow analysis	yes	parametric analysis	yes	yes	updates supplied periodically on the Maui Solar Software site; you can add modules and inverters	online help file, training videos
lifecycle cost calculations including electricity purchased from utility, electricity sold to utility, O&M costs, rebates, tax credits, depreciation; cash-flow analysis	can be copied and pasted into Excel	parametric analysis	n/a	n/a	n/a	user manual provided with software
economic efficiency and cash-flow analysis	yes	tilt, inter-row spacing, inverter loading	yes	yes	updates to the database are supplied by manufacturers; the program can be set to check for updates at start up	limited help file available with program; training available
considers energy costs, feed-in tariffs and system financing	yes	tilt, orientation, inter-row spacing, inverter loading	yes	yes	updated approximately once a year, usually with the release of a software update; you can define additional components or import individual component files received from other sources	detailed help file available with program, FAQ on Web site, no user manual
basic calculation of energy value	8,760 report is output as text that can be pasted into an Excel file	n/a	n/a	n/a	n/a	online documentation and support available
basic calculation of energy value	n/a	n/a	n/a	n/a	n/a	limited help file provided available with program, additional online documentation and support available
detailed cash-flow analysis, sensitivity and risk analysis	program is Excel based	n/a	yes	n/a	manufacturer must contact RetScreen	online manual, detailed help file, online training courses
detailed cash-flow analysis for residential, commercial and utility scale projects; focused on the US market; sensitivity and statistical analysis tools	yes	numerous production and financial optimization tools, parametric analysis	yes	yes	CEC module model (NREL maintains a library of CEC-approved modules), SAM can sync with the most recent library, additional modules can be added by contacting NREL; library of inverter coefficients is updated regularly as the CEC inverter database is updated	extensive user manual, detailed help file, online user group, email support

Courtesy maui-solarsoftware.com



PV-DesignPro parametric analysis This chart was created using the default load profile available in PV-DesignPro and the PG&E A-6 rate schedule that is preloaded in the program. The lowest electric bill for a customer in San Francisco, CA, is achieved at a module tilt of 30° and an azimuth of 10°. (System specifications: 1,376 Mitsubishi PV-UD185MF5 modules; one Xantrex PV225 inverter.)

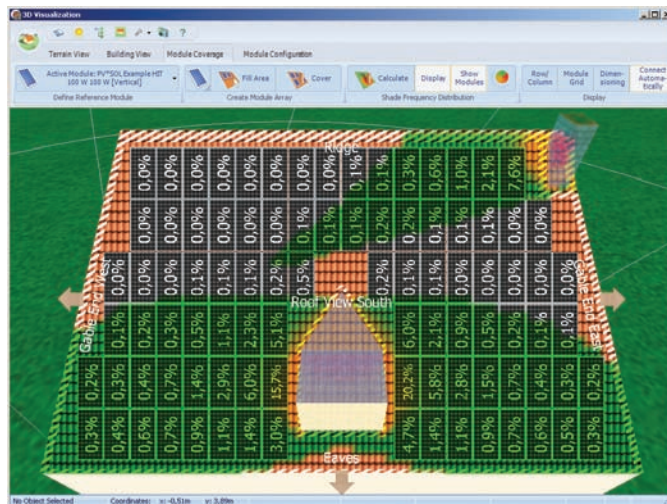
compare the financial benefits that may result from switching rate schedules when installing a PV system.

PV*SOL

PV*SOL is produced by Valentin Software, based in Germany. The program is widely used in the European market, and Valentin has begun efforts to increase market share in the US. These efforts include a 2010 release of an Americanized version of both PV*SOL and its most advanced tool, PV*SOL Expert, that use American numbering conventions and a North American product database. PV*SOL contains an extensive database of modules and inverters that is frequently updated. The program can be set to automatically check for updates to the database on startup. You can account for shading by creating or importing a horizon profile. Derate factors, such as mismatch, soiling, dc voltage drop, module tolerance, and losses across diodes and connections, are all considered.

At the start of each session you are given the option to use a Quick Design tool. After you select a specific type of module, the number of modules that are to be installed and an inverter brand, the program calculates all of the possible stringing combinations. The options are ranked based on how efficient they are at using inverter capacity. This is useful when trying to determine the best way to use numerous string inverters on a project.

PV*SOL stands out in its ability to model multiple arrays and multiple inverters in the same simulation, something not possible with most tools. Each array can be specified independently of the others, including module type, array tilt and azimuth, and single or multiple inverters. Derate factors and horizon profiles can also be specified independently for each



Courtesy valentin-software.com

PV*SOL shading simulation This PV*SOL screen capture is color-coded to indicate the amount of shading across the roof. The numbers on the modules indicate the shading loss for each. A US version of PV*SOL will be available in 2010.

array. On complex projects with multiple buildings, this can significantly reduce the simulation time.

PV*SOL Expert contains a 3D shade modeling environment in which a building can be defined that includes typical features such as gables and chimneys. Other objects that may shade an array, such as trees and additional structures, can be added to the model. You can then run a simulation that color-codes the roof according to the amount of shade an area receives. This simulation also lets you arrange modules on the roof and see the shading loss for each one, as shown in the screen capture above.

Although many of the advanced tools available in both versions of PV*SOL are geared toward the simulation of roof-mounted systems, the program also contains options for vertical single-axis tracking as well as dual-axis tracking. The program does not have an option for horizontal single-axis tracking.

PVSYST

PVsystr, developed at the University of Geneva, Switzerland, is currently the hot name in production modeling. It is the primary tool used by independent engineers who are brought in to verify production numbers for investors. The program contains a large database of modules and inverters for component selection. PVsystr considers many of the system losses as the other modeling tools do. Where it stands out is its treatment of shading and soiling.

You have the ability to enter a different soiling factor for each month in PVsystr, which more accurately reflects real-world conditions. The program can quickly model the effects of inter-row shading through

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an option called *unlimited sheds* that calculates when the system experiences inter-row shading based on the array parameters and on the location and orientation of the array. PVsyst also provides you with a 3D CAD-like environment in which a more complex model of a PV system and the nearby surroundings can be created. Once an array is defined, it can be broken into strings, and the effect that shading has on a string can be specified.

PVsyst provides numerous array configuration options. To simulate tracking, you can define the important characteristics such as single or dual axis, maximum and minimum tilts, the spacing between rows or arrays, and whether or not the tracker employs backtracking. (*Backtracking* is a tracking strategy controlled by a microprocessor that adjusts the array tilt to constantly avoid inter-array shading, especially early and late in the day.) PVsyst can simultaneously model systems that comprise more than one size or type of inverter, as well as arrays with two different tilts and azimuths connected to a single inverter.

What makes PVsyst such a valuable tool is not that it has a more accurate model for PV or solar cell production than the other production-modeling systems available, but rather its unique ability to control and accurately define many of the other factors that are involved in production modeling. The report that PVsyst produces, and in particular the diagram showing system losses, is especially valuable. A new version of the program, PVsyst 5.0, was released in June 2009 and updates to the program are released regularly on the PVsyst Web site (see Resources).

COMPARISON OF PV PRODUCTION MODELS

We use the production-modeling tools just discussed to simulate the annual energy yield for different system designs. In this section we compare the tools' production estimates for theoretical systems of different technologies and perform two case studies to compare the modeling tools' production estimates to measured production. These tools are evaluated in the following model-to-model comparisons:

- PVWatts, v. 1
- PVWatts, v. 2
- PVsyst v. 4.37
- SAM, Sandia PV performance model and Sandia inverter performance model
- SAM, CEC PV performance model and Sandia inverter performance model
- PV*SOL 3.0, release 7
- PV-DesignPro, v. 6.0

“PVsyst provides more conservative results and is more powerful at covering complex issues such as shading.”

—Manfred Bächler,
chief technical officer,
Phoenix Solar

In order to provide an understanding of the relative performance of each tool in different scenarios, we compare the performance-modeling tools' production estimates for crystalline silicon PV modules on a fixed-tilt array, a single-axis

tracking array and a dual-axis tracking array, as well as thin-film modules on a fixed-tilt array.

To perform the simulations in each modeling tool across the three mounting systems and the two module technologies, we input specifications for four generic systems, as follows:

CRYSTALLINE SYSTEMS

Modules: Sharp ND-216U2 (216 W STC, 187.3 W PTC)

Inverter: Xantrex GT250 (250 kW, 96% CEC efficiency)

Array: 1,400 modules (302.4 kW STC), 100 strings of 14 modules each

Installation #1: Fixed-tilt ground mount, 0° azimuth (true south), 30° tilt

Installation #2: Single-axis tracking (north-south), 0° azimuth (true south)

Installation #3: Dual-axis tracking

THIN-FILM SYSTEM

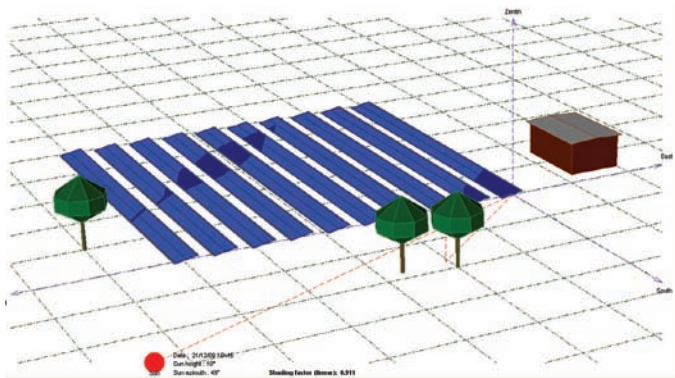
Module: First Solar FS255 (55 W STC, 51.8 W PTC)

Inverter: Xantrex GT250 (250 kW, 96% CEC efficiency)

Array: 5,028 modules (276.5 kW STC), 838 strings of 6 modules each

Installation: Fixed-tilt ground mount, 0° azimuth (true south), 30° tilt

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PVsyst 3D model The near shading scene function in PVsyst is used to calculate the impact of obstructions like adjacent trees or structures on system performance. In this case, the effects of shading are modeled on a vertical east-west single-axis tracking system.

The systems are sized by starting with a chosen inverter, dividing the ac power rating by the CEC-rated efficiency, then dividing by the module's PTC rating. The resulting number of modules is rounded up to a whole number of strings.

MODELING-TOOL PARAMETERS

We use the default derate parameters for each modeling tool—with the exception of SAM, for which we match the derate factors to those from PVWatts for consistency. Table 1 lists the derate parameters used in the various modeling tools.

Each PV system is located in San Francisco, California. NREL TMY2 data for that location are used in the modeling. For the purposes of modeling with PVWatts v. 2, the 94124 zip code is used to identify the 40-by-40 km grid.

Each tool's default POA radiation model is used. This means that simulations performed with PVWatts v. 1 and v. 2, SAM and PV-DesignPro use the Perez et al. model; PVsyst and PV*SOL use the Hay and Davies model.

To maintain consistency between tools when modeling tracking, we did not use PVsyst's capability to model the back-tracking or shade avoidance. In addition, the horizontal single-axis tracking design was not modeled in PV*SOL, as that tool can model only a vertical single-axis tracking design.

RESULTS OF MODEL-TO-MODEL COMPARISONS

The results of the modeling comparisons are presented in terms of *specific yield* in Graph 1. Specific yield is the production in kWh with respect to the STC system size in kW. In other words, it is energy divided by nameplate power. This allows for a more direct comparison between different technologies.

In reviewing the results presented in Graph 1 and the source data, we make the following observations about the estimates that each of the tools generated:

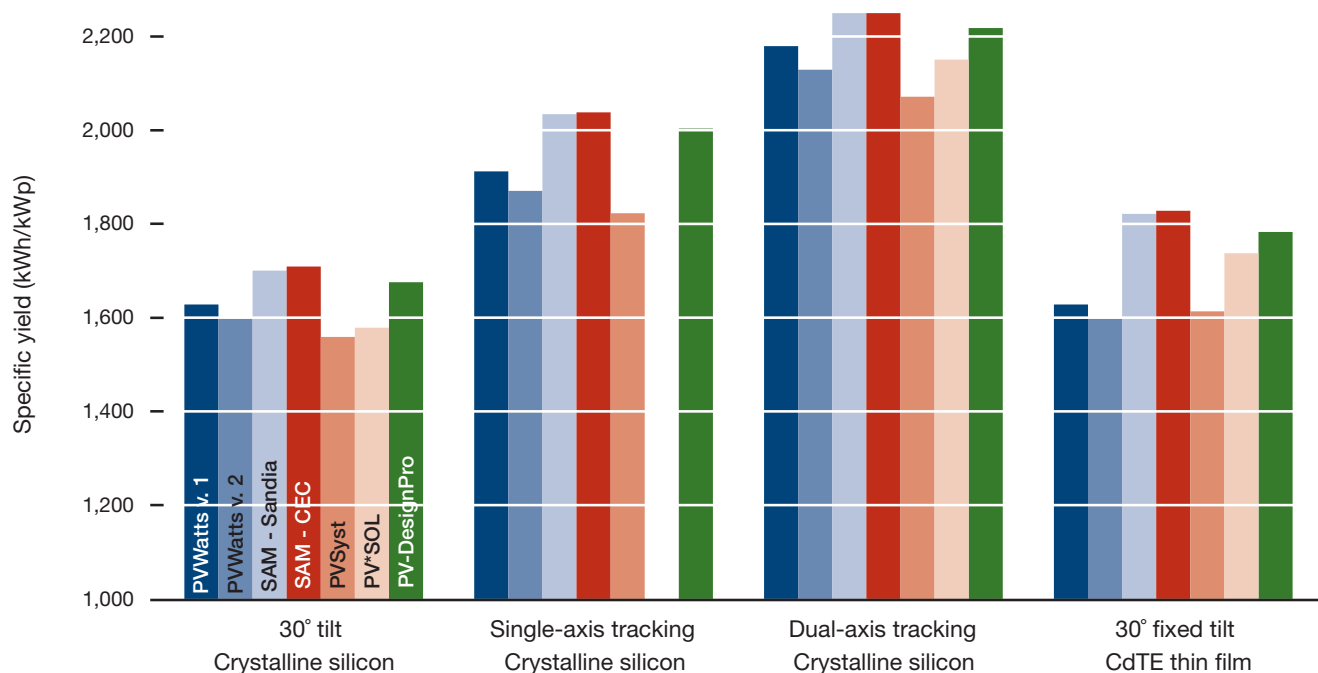
- For any single scenario, the discrepancy between the maximum and minimum production estimate ranged from 9% to 14%; the average difference was 11.5%.

- The largest discrepancy between production estimates was 14% for the thin-film scenario. This reflects the greater level of uncertainty associated with modeling the performance of thin-film modules.
- With the exception of the thin-film scenario, PV*SOL and PVWatts (v. 1 and v. 2) consistently produce estimates that fall between those for SAM and PV-DesignPro at the high end and PVsyst at the low end.
- In the thin-film scenario, the relatively lower estimates for PVWatts v. 1 and v. 2 are expected due to the inability of the tool to accurately model thin-film performance. What is unexpected is that the PVsyst estimate is similar to those from PVWatts v. 1 and v. 2.
- The estimates of the two SAM models were consistently the largest or most aggressive estimates. Using the CEC PV performance model, SAM generally estimated a 1% higher annual production than it did when using the Sandia PV array performance model. The small percentage suggests that the difference in module performance models is small, in the context of a full-system simulation.
- PV-DesignPro consistently estimates between 1.5% and 2% below the SAM models, but still significantly higher than most other tools' estimates. By default, PV-DesignPro considers MPPT efficiency and dc wire loss only. We expect that its production estimates would be lower if consistent derate factors were applied.
- PVsyst consistently produced the smallest or most conservative production estimates. Comparing the PVsyst loss diagram that the software generates with the simple derate factors for other modeling tools leads us to believe that this result is largely due to the module performance model within PVsyst. Differences in module and inverter characteristics within the tool's databases may also contribute to this result.
- PVWatts v. 1 estimates an average of 2% more annual production than v. 2. We believe the difference is attributable

Derate Factors Model-to-Model Comparisons

	PVWATTS v. 1 & v. 2	SAM (CEC & Sandia models)	PVsyst	PV*SOL	PV-DesignPro
PV module nameplate	0.95	-	0.97	1	1
Inverter & transformer	0.96	MOD	MOD	MOD	MOD
Mismatch	0.98	0.98	0.98	0.98	1
Diodes & connections	0.995	0.995	MOD	0.995	1
dc wire loss	0.98	0.98	MOD	MOD	.99
ac wire loss	0.99	0.99	1	1	-
Soiling	1	1	1	1	1
Shading	1	MOD	1	1	1
Sun tracking	1	1	MOD	1	1
MPPT efficiency	-	-	-	-	0.95

Table 1 Derate factors for each program are translated to a decimal value for comparison, matching the convention used in PVWatts. "MOD" denotes that the parameter is modeled within the tool, rather than reduced to a single derate factor.



Graph 1 This graph shows the annual specific yield estimated by the different PV production models for the four comparison PV systems. Absent data in the single-axis tracking example is due to the fact that PV*SOL does not model vertical (north-south) tracking.

to the modification of weather data in PVWatts v. 2 to improve geographic resolution; as such, other sites may produce dissimilar results.

CASE STUDIES: COMPARING MODELING TOOL OUTPUT TO PRODUCTION DATA

To compare predicted performance with the measured performance of actual systems, we perform two case studies of PV systems in operation. Case Study #1 is a fixed-tilt hybrid monocrystalline /amorphous silicon installation on a rooftop in Escondido, California. Case Study #2 is a fixed-tilt carport installation with amorphous silicon thin-film modules in Santee, California. Both projects have monitoring equipment that includes measurement of insolation; as such, both the energy produced by the systems and the insolation available to the systems can be compared to simulations.

For the case studies, we reduced the number of tools used. This is due to the similarity in results observed in the comparisons between two pairs of PVWatts and SAM models. For PVWatts, only v. 2 was used in the case studies. For the two SAM models, we used the Sandia PV array performance model for Case Study #1 and the CEC performance model for Case Study #2; this is due to the availability of modules in the respective databases.

MODELING PARAMETERS

Weather data. The meteorological data for all simulations are NREL TMY2 data for San Diego, California, with the exception of the PVWatts v. 2 simulation, which uses modified data based on the zip code for each system.

Shading. Each modeling tool addressed inter-row shading as follows:

- In PVsyst, by utilizing the “unlimited sheds” modeling technique;
- in SAM by using the 12-by-24 shading matrix;
- in PVWatts by entering the shading loss resulting from the PVsyst simulation; and
- in PV*SOL and PV-DesignPro by creating a horizon profile.

No additional shading is considered, because the arrays are largely shade-free.

Soiling. This is modeled in PVsyst at 1.5% per month, accumulating from month to month when the average rainfall in that month was not significant. When rainfall was significant or the system was cleaned, the soiling factor was reduced to 1.5% for that month. Case Study #1 was not cleaned and the resulting annual soiling loss was 4%. Case Study #2 was cleaned at the end of June, and the resulting annual soiling loss was 3.1%. These annual soiling losses are used in all modeling tools.

Other. Except as noted below, all other derate factors are as per Table 1:

- In PV*SOL a module tolerance of -3% is specified.
- In PV-DesignPro MPPT efficiency is modeled as 98%; an array voltage derate factor of 0.975 is used to account for module mismatch and losses in diodes and connections; wiring losses are set at 3%.

As these systems are both in their first 12–18 months of operation, no module degradation is considered. System availability is also not considered, because each system had no significant downtime.

CASE STUDY #1

The first case study is a 78.4 kW roof-mounted array in Escondido, California, consisting of Sanyo HIP-200BA3 hybrid monocrystalline/amorphous silicon modules that are tilted at 10° and oriented directly south (0°). The array is wired with seven modules per source circuit, and the resulting 56 source circuits are connected to a PV Powered PVP75KW-480 inverter. The system has been in operation for just over 18 months with no significant downtime since being commissioned. The site is relatively new construction and is located in an area where further construction is occurring. As a result, soiling is expected to have a significant impact on the system's performance. In addition, there is a local wastewater ordinance restricting the owners' ability to clean the system. Therefore, it has not been cleaned since it was commissioned.

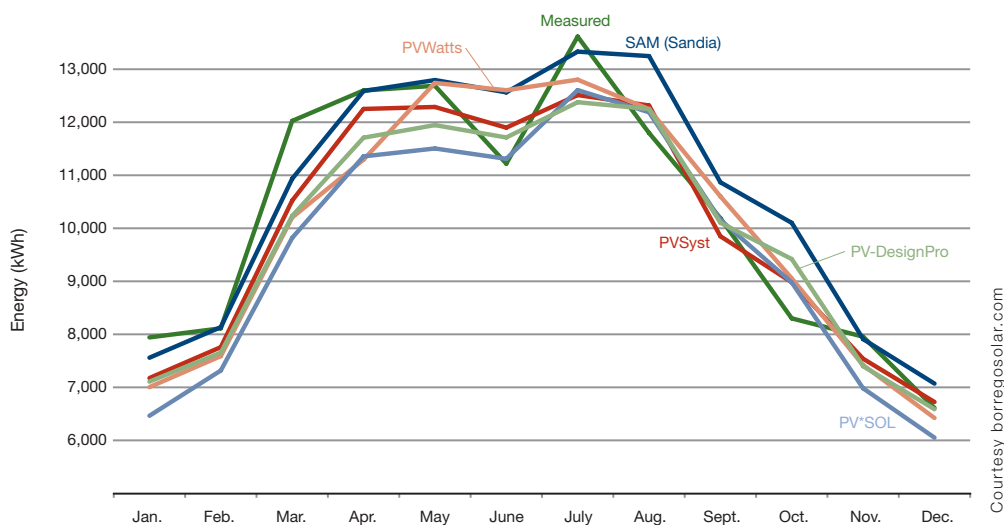
Results. The modeling results for Case Study #1 are presented in Table 2. They show that measured insolation is approximately 10% greater than modeled. This is consistent across the different tools, indicating that they perform comparably in modeling weather data. The estimated production, however,

is close to the measured production, with the exception of the PV*SOL modeling tool. The combination of the modeled insolation being lower than measured, but modeled production approximately matching what was measured, indicates that the modeling tools will significantly overestimate system production if an average or typical weather year were to occur. Our interpretation is that the system is underperforming with respect to the modeling tools' predictions. This underperformance is consistent with reports from the project site indicating that significant soiling is reducing production.

Graph 2 shows that the monthly production estimates and measured production values are within the same range and follow the same trend over the course of the year, with some exceptions. The most significant exception is the drop in measured production in June. When reviewing the insolation data, we observe an equivalent drop. Therefore the system is performing as expected. (This drop in June is also observed in Case Study #2.)

With the exception of June, the modeling tools appear to have produced estimates in reasonable

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Graph 2 This graph shows the monthly energy production in kWh for the measured and modeled system in Case Study #1.

Case Study #1: Measured-to-Modeled Comparison

	Measured	PVsyst	SAM (Sandia)	PVWatts	PV*SOL	PV-DesignPro
Insolation (kWh/m ² /year)	2,178.6	1,977.3	1,981.2	2,004.8	1,911.8	1,984.6
Delta to measured (%)	0.0%	-9.2%	-9.1%	-8.0%	-12.2%	-8.9%
Production (kWh)	123,058	119,816	127,107	119,986	114,736	118,502
Delta to measured (%)	0.0%	-2.6%	3.3%	-2.5%	-6.8%	-3.7%

Table 2 This table presents the measured and estimated annual insolation and production values for Case Study #1 as well as the percent difference of measured-to-modeled values.

agreement with the measured data. However, when you examine Graph 2 closely, you can see that—with the exception of June—the measured data either exceed or are equal to the estimated data from January to July. It is reasonable to suppose that if insolation in June had not been relatively low, the production that month would also have exceeded the predictions. From August through October, however, the measured data fall below nearly all of the modeled estimates. Only one modeled data point—that for PVsyst in September—is lower than the measured data. This indicates the impact of soiling on production through the dry summer season in San Diego County. The PVsyst capability to model soiling on a monthly basis captures the behavior. The estimated production values in November and December are similar to the measured values.

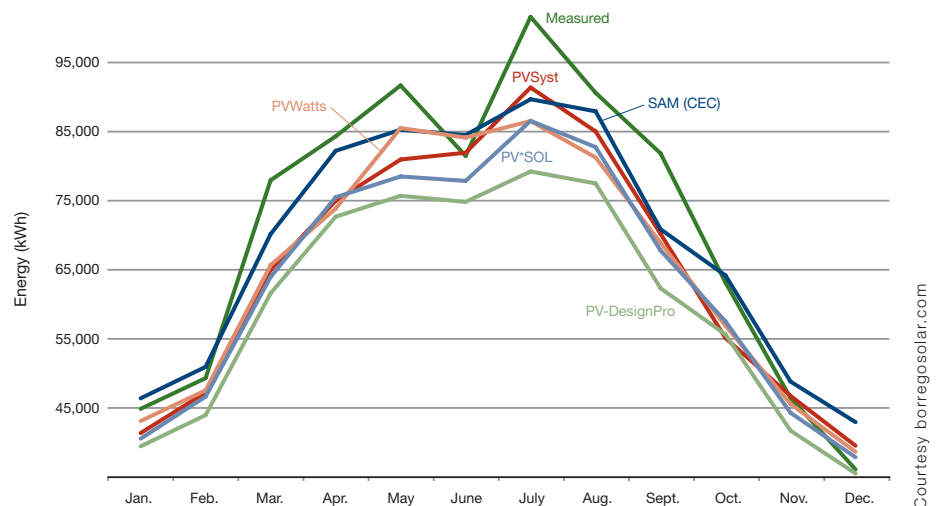
CASE STUDY #2

The second case study is a 481.5 kW carport-mounted array in Santee, California, consisting of Kaneka G-SA60 single-junction amorphous silicon thin-film modules, tilted at 5° and oriented 27° west of true south. The array is wired with five modules per source circuit, and the resulting 1,605 circuits are connected to two Xantrex GT250-480 inverters. The carport is actually an RV parking shelter and has a roof deck immediately below the modules, which reduces airflow and increases module temperature. The system has been in operation for just over 12 months with no significant downtime since being commissioned.

Results. The modeling results for Case Study #2 are presented in Table 3. They show that measured insolation is approximately 5% lower than modeled. This is consistent across the different tools, indicating that they model weather data comparably. The estimated production, however, varies widely, ranging from 3% below the measured value for SAM to 15.2% below for PV-DesignPro.

The wide variation is an indicator that modeling the performance of thin-film modules is more complex and presently less accurate than modeling performance for crystalline silicon modules.

PVWatts is limited in its ability to model modules other than crystalline silicon. Given that amorphous silicon modules are used in this case study, we account for this limitation in PVWatts by applying a correction factor to the STC system size specified in the PVWatts model. The correction factor is determined by comparing the PTC to STC ratio for the Kaneka G-SA60 module to that for a reference crystalline module, in this instance the Sharp ND-216U2. The PTC to STC ratio is 10% higher for the Kaneka module; as a result, the system size modeled in PVWatts is increased by 10%. The results shown in Table 3 indicate that the adjusted PVWatts v. 2 results are similar to those for the other tools. This approach is similar to the one used by the Los Angeles Department of Water and Power in its incentive program. While this appears to produce reasonable results, more effective tools are available for modeling thin-film module performance.



Graph 3 This graphs shows the monthly energy production in kWh for the measured and modeled system in Case Study #2.

Case Study #2: Measured-to-Modeled Comparison

	Measured	PVsyst	SAM (CEC)	PVWatts	PV*SOL	PV-DesignPro
Insolation (kWh/m2/year)	2,037.6	1,944.1	1,922.7	1,956.4	1,855.7	1,918.3
Delta to measured (%)	0.0%	-4.6%	-5.6%	-4.0%	-8.9%	-5.9%
Production (kWh)	849,136	779,192	823,635	777,359	759,531	719,869
Delta to measured (%)	0.0%	-8.2%	-3.0%	-8.5%	-10.6%	-15.2%

Table 3 This table presents the measured and estimated annual insolation and production values for Case Study #2 as well as the percent difference of measured to modeled values.

Graph 3 shows that the monthly estimates for production and the measured production follow the same broad trend, in terms of an increase in production during the summer. As in Case Study #1, the one instance where measured and modeled production do not track one another is the drop in measured production in June. Again, the insolation data reveal a similar reduction, and thus the behavior is as expected.

While generally predicting near the average of the other modeling tools, PVsyst has the highest production estimate in July. This is due to PVsyst's ability to model month-by-month soiling factors. The soiling factor was reduced from 6% for June to 1.5% for July when scheduled cleaning was carried out, and the resulting production increase is reflected in the production graph. Other tools also show a similar trend, but this is simply in proportion to the increased insolation available in July.

THE VALUE OF PRODUCTION MODELING

Production modeling impacts many aspects of PV project development. During the sales cycle, performance estimates are necessary for determining project capacity and lining up financing. These estimates are also used during the design and engineering phase to make informed design decisions that optimize PV system performance. During operations, production modeling is used to evaluate system performance to ensure appropriate production. Production modeling also has a key role in the evaluation of new products and technologies.

System sizing. Production estimates of varying complexity are essential in determining the appropriate size system to build. In simple situations where customers are trying to offset a portion of their annual energy bill, a back-of-the-envelope production estimate may suffice. However, if customers are trying to zero out their electric bill or if TOU rate schedules are in play, the method used to estimate production needs to be more precise, more sophisticated. You can have more confidence in design decisions by modeling with tools that use location-specific weather data and produce hourly estimates of production.

Financials. Revenue from energy production is a major force, if not *the* driving force in PV project development. In an environment where the majority of PV projects, particularly larger projects, are not purchased outright but financed through complex deals, the value of each kWh generated cannot be understated. Incentives based on kWh rather than kW—such as the California Solar Initiative Performance Based Incentive program or one of many solar renewable energy credit programs—can double or triple the simple value of a kWh, exceeding \$0.30/kWh.

Given the potential value of each kWh, system production has a huge impact on the revenue a project generates. If production is significantly under- or overestimated, the effects can be serious on the project at hand, on future deals and on the industry as a whole.

Underestimated production can cause any number of development issues, perhaps misrepresenting project viability or resulting in an oversized system. Underestimated production may prevent a project from being developed that might otherwise have been attractive. Or it could push a customer toward a deal with a developer whose production estimate is higher. If an oversized system results, the excess electricity generated may have to be given away to the utility without compensation.

Overestimated production may result in changes to the financial structure of the project. This is true when the commissioned system cannot meet the performance requirements established through production modeling. Production guarantees that are based upon an overestimated production model can lead to financial penalties for the party guaranteeing the system performance. An underperforming asset may not have the market value that an owner had planned on when committing to the project terms.

Whether used by investors examining revenue streams, integrators looking to guarantee that revenue, or end customers looking to offset their utility bills, accurate energy production estimates are crucial to all parties in the successful deployment of a solar energy project. Given this importance, investors rarely evaluate production estimates themselves. Instead, independent engineering firms with extensive production-modeling experience are generally relied upon. Typically, the independent engineering firm also verifies system performance following commissioning.

System design. Production-modeling tools play an essential role in maximizing the production or financial return of a PV system. The first step is making a decision about what technology to deploy based on a given location or a set of financial considerations. Different climates and locations affect the output of various technologies, such as crystalline silicon versus thin-film PV or single- versus dual-axis trackers. The times of the day and seasons of the year when these technologies produce power also vary. A technology that has the best financial return in one location or under a given rate schedule may not be the best choice in other circumstances.

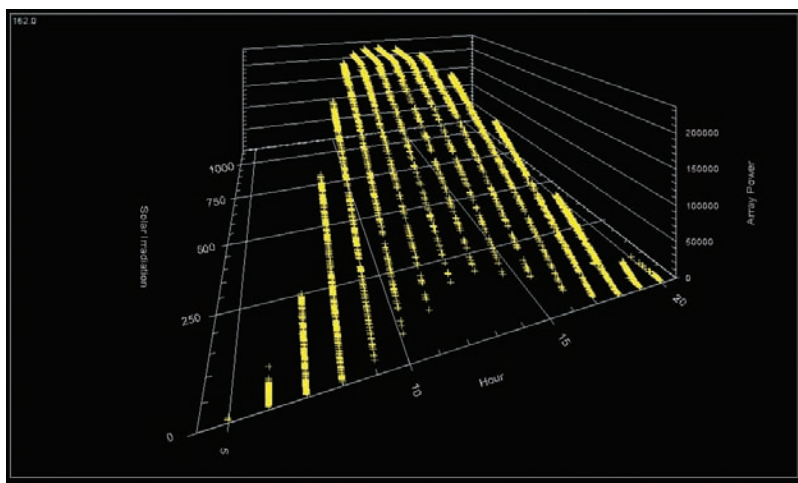
“Currently, all the models lack the seriousness that can be provided only by having skin in the game. Once there is a tool out there that people put money behind, the entire solar industry will get far more serious and real.”

—Fred Unger, president,
Heartwood Group

Once a technology choice has been made, modeling tools allow you to optimize the array layout. A general rule of thumb holds that the optimal configuration to maximize annual production is a tilt angle equal to the site's latitude with a

due south azimuth. While this rule would be true for a single-plane array under ideal circumstances, inter-row shading and local weather variations can skew the optimum configuration. Modeling tools can be used both to find the optimal configurations and to look at what effect a nonoptimal configuration would have. For fixed-tilt systems, modeling tools can be used to determine the effects of inter-row shading. They also help to determine the balance between the increased capacity allowed by smaller shade setback distances and the decreased production. For tracking systems, modeling tools can help you make decisions about the spacing of arrays or whether backtracking is a valuable option. The 3D shade simulations can be used to place arrays in areas where they are least impacted by shading from trees or roof obstructions.

Performance-modeling tools also allow you to make informed decisions about inverter sizing. For example, if a building can accommodate an array rated at 500 kW STC, should you use a 500 kW inverter or a 350 kW inverter? Using a modeling tool that accounts for power loss due to clipping allows you to compare the value of the lost power



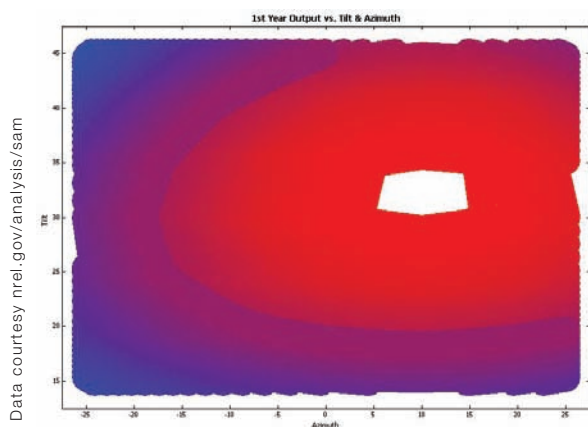
Inverter clipping This PV-DesignPro scatter plot has one data point for each hour of the year. It illustrates how much power clipping results from overloading a Xantrex PV225 inverter with a 384.8 kW array (2,080 Mitsubishi PV-UD185MF5 modules) for a system in San Francisco, CA, with a 25° tilt and a 0° (true south) azimuth.

Courtesy maui-solarsoftware.com

The Dollars Are in the Details

The following production-modeling examples, which seek to correlate annual production to system tilt and azimuth, show the importance of using modeling tools that account for detailed system variables.

Example 1: SAM. An optimization run using SAM for a 250 kW system in San Francisco, California, at a latitude of 37.6°, shows that annual production is maximized with a tilt

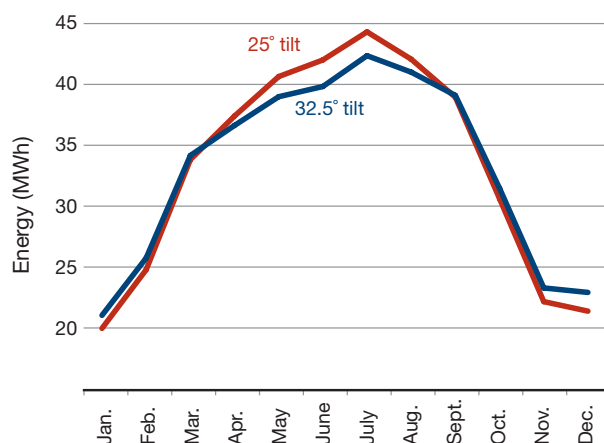


Graph 4 This contour graph was created by SAM and shows the relationship of energy production to tilt and azimuth for a modeled PV system in San Francisco, CA.

of 32.5° and an azimuth of 8°, where true south is 0° and positive values indicate an azimuth that is west of south. See Graph 4 for a representation of this result. The SAM optimization assumes no shade. However, most large systems are composed of numerous rows spaced at a calculated distance, and are often designed to have inter-row shading before 9am and after 3pm on December 21. Unfortunately, SAM does not provide an easy method for defining inter-row shading.

Example 2: PVsyst. Production numbers run in PVsyst, which provides an inter-row shading option, show that for systems with an 8° azimuth and inter-row spacing that keeps the array shade free between 9am and 3pm on December 21, a tilt angle of 25° actually produces slightly more annual power than one tilted at 32.5°. This is illustrated in Graph 5, which shows the monthly kWh production for 25° and 32.5° tilt angles, as modeled by PVsyst. Tilting the array at 25° has additional benefits: Production is weighted toward the summer months when power is generally more valuable; the system covers a smaller area; and less racking material is required.

In this case, using the data from SAM would appear to result in a less productive, more expensive system. You could run additional comparisons to optimize the system for total production, TOU weighted production or other system metrics. ●



Graph 5 This graph was produced using monthly energy production numbers generated by PVsyst. It indicates that for a system with an 8° azimuth in San Francisco, CA, a 25° tilt generates more energy than a 32.5° tilt, especially in the summer.

over the life of the system when using the 350 kW inverter to the increased upfront cost of installing the 500 kW inverter. You can run the same type of analysis to make the decision between a single inverter or multiple inverters for arrays with different orientations.

Operations. Production-modeling tools can also be used to evaluate a PV system's long-term performance. Accurate production modeling establishes a relationship between the irradiance available to the system and the electricity produced by the system. This ratio is applied to the measured irradiance and used to determine the expected production. This result can be compared to the measured production to determine whether the system is performing as expected. This can be done in real time, typically using Web-based analysis tools for

viewing the data from the system, or retrospectively over a given time, typically monthly or annually. Accurate modeling of all of the system parameters is critical to the effectiveness of this technique, as are accurate measurements of the irradiance and production values.

CONCLUSIONS

Based on our evaluations, the radiation model components of the evaluated tools perform consistently, predicting similar POA irradiance from the same weather data. In terms of production estimates, SAM is the most aggressive modeling tool and PVsyst the most conservative. There is an average of 9% difference between their estimates.

Given the importance of accurate energy production estimates, the sophistication and capabilities of modeling tools *must* continue to evolve along with the solar industry. At this stage, an ideal tool might combine the following features: the Sandia PV array performance model; a component database updated as frequently, or more often, than the CEC database; PVsyst's control over system and location variables; and SAM's ability to perform financial, parametric and statistical analyses. Throw in the ability to define 3D layouts in a CAD-like environment—as in PVsyst—and to load shade readings taken in the field—as with Solmetric's PV Designer software and its SunEye tool—and you would have it all.

In the end, production-modeling tools are only as good as the person who uses them. The choice of derate factors can easily shift a production estimate by 5% or more. That

“New technologies and applications create new challenges for modelers. There is a continuing need for development and validation of models for diverse technologies, applications and climates to ensure model accuracy and to quantify uncertainty.”

—Chris Cameron,
project lead for systems modeling,
Sandia National Laboratories

said, for accurate simulations, it is important to have a tool that gives you as much control as possible over the factors that affect production. Currently, PVsyst is the tool that stands out, due to its ability to account for shading from a variety of sources and to vary soiling definitions

over the course of the year as well as its flexibility to model a large number of different configurations.⊕

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RESOURCES

Production-modeling software

HOMER / 720.565.4046 / homerenergy.com

Polysun / 415.671.6292 / velasolaris.com

PV Designer / 707.823.4600 / solmetric.com

PV-DesignPro / mauisolarsoftware.com

PV F-Chart / 608.255.0842 / fchart.com

PV*SOL / 888.786.9455 / valentin-software.com

PVsyst / +41.22.379.0650 / pvsyst.com

PVWatts v. 1 / 303.275.3000 / rredc.nrel.gov/
solar/codes_algs/PVWATTS/version1/

PVWatts v. 2 / 303.275.3000 / rredc.nrel.gov/
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314.447.8010 / elsevier.com

Go Solar California / gosolarcalifornia.
ca.gov/equipment (Inverter performance test
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Glossary of Solar Radiation Resource Terms /
rredc.nrel.gov/solar/glossary



Tuesday, June 04, 2013

Pam Brenner – Town Administrator
1 Grove Street
Peterborough, NH 03458

Re: Letter of Support for Photovoltaic System at Waste Water Treatment Facility at 58 Water Street Peterborough, NH

Dear Pam:

I wanted to summarize our intent and key deal points within this Letter of Intent (*LOI*) which will be memorialized in an Option to Lease Agreement and a Power Purchase Agreement as outlined within this agreement in the future. The *LOI* is for the leasing of your land located at **58 Water Street in Peterborough, NH, containing approximately 4 acres**, identified in Appendix A (the “*Premises*”) owned by you (the “*Lessor*”). Borrego Solar Systems, Inc. (*Borrego*) is pursuing a transaction with a third party that would result in (i) the installation and operation of up to a 1 Megawatt (MW) ground mounted solar facility at the above referenced Premises at Borrego’s cost; (ii) the sale of the energy produced by the facility to the Town of Peterborough; and (iii) a lease for the use of the land of the Premises during the operation of the facility.

QUALIFYING CONDITIONS

This *LOI* as set forth below will allow Borrego to engage in further development activities which include but are not limited to applying for a grant through the NH PUC further evaluation of the Premises for the installation and operation of the facility, finalize our agreement through a long-term PPA, and begin negotiating option and lease documents. Should Borrego be successful in receiving the NH grant award, executing a PPA with the general terms herein and permitting the project, we will exercise this option and engage in a site lease agreement on the general terms herein:

Borrego Solar Systems, Inc.

1115 Westford Street

Lowell, MA 01851

www.borregosolar.com



BORREGO SOLAR

PPA Terms:

- *Rate:* 8 cents/kWh with a 1% annual escalator
- *Term:* 20 years with (2) 5 year extension options.
- *Total Grant Award Required:* TBD
- *Commercial Operation Date:* Shall be defined as the date the system begins generating energy for sale.
- *Environmental Attributes:* all environmental attributes generated by the facility are the property of Borrego.
- *Facility:* Upon expiration of the PPA, the PPA will either be renewed at an agreed upon rate, or the system may be purchased by the Town of Peterborough at fair market value, or the system will be removed by tenant at tenant's sole cost.
- *Assignment:* Borrego may assign its rights and obligations under the PPA to a third party buyer of the facility subject to the approval of the Town of Peterborough, which approval shall not be unreasonably withheld.
- *Interconnection:* Approximately half of the project will be connected behind the existing utility meter at the WWTF, and the other half of the project will be connected behind the meter at the middle school directly across the street.

Option to Lease Terms:

- *Proposed Rent:* \$0 – The financial benefit is passed on to the Town of Peterborough in the form of a reduced PPA rate.
- *Commercial Operation Date:* Shall be defined as the date the system begins generating energy for sale.
- *Use:* Borrego shall have the right to construct, operate, access, monitor and maintain the facility, including all panels, inverters, fuses, transformers, wiring, racking, meters and other improvements related to the facility.
- *Costs:* Borrego shall be responsible for all costs and the performance of all work related to the design, construction, operation, monitoring and maintenance of the facility.
- *Facility:* Upon expiration of the lease, the lease will either be renewed at an agreed upon rate, or the system may be purchased by the Town of Peterborough at fair market value removed by tenant at tenant's sole cost.
- *Assignment:* Borrego may assign its rights and obligations under the lease to a third party buyer of the facility subject to the approval of the Lessor, which approval shall not be unreasonably withheld.

Borrego Solar Systems, Inc.

1115 Westford Street

Lowell, MA 01851

www.borregosolar.com



BORREGO SOLAR

Please indicate your willingness to start working together on the **58 Water Street Peterborough, NH solar project** by signing as indicated below. We look forward to developing this project with you.

Very Truly Yours,

Joe Harrison
Project Developer
Borrego Solar Systems, Inc.
c. 207-432-1317

ACCEPTED AND AGREED

Town of Peterborough, NH

By:

Pamela F. Benner

Date

6/26/2013